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EXACT RELAXATION TIMES AND DYNAMIC FUNCTIONS FOR DILUTE POLYMER SOLUTIONS FROM THE BEAD/SPRING MODEL OF ROUSE AND ZIMM

A. S. Lodge, et al

Wisconsin University

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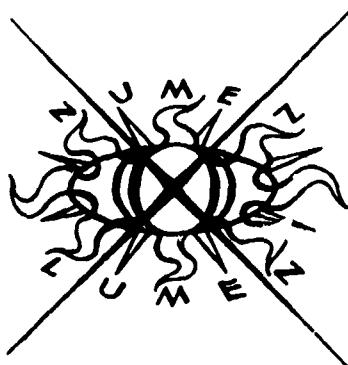
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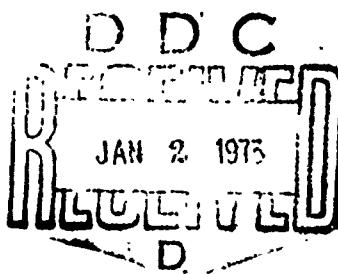
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ABSTRACT

A UNIVAC 1108 Computer has been used to obtain exact values for λ_p ($p = 1, 2, \dots, N$), the non-zero characteristic values of Zimm's matrix HA, for values of N (the number of Gaussian springs per molecule) up to 300; values previously published did not go above $N = 15$ (Thurston and Morrison). For future comparison with elastic and viscous properties of very dilute polymer solutions measured in steady and in oscillatory shear flow, several useful functions of the λ_p are computed and tabulated for parameter values in the ranges $2 \leq N \leq 300$, $0.05 \leq h^* \leq 0.3$, where h^* ($= hN^{-1/2}$) is a dimensionless "friction constant"; h denotes the "hydrodynamic interaction parameter" of Zimm. For selected parameter values, certain of the functions are compared graphically with the corresponding functions given by Tschoegl on the basis of approximate calculations using an indefinitely large value for N . The present calculations differ from those of Zimm and Tschoegl in only two ways: finite values of N are used (instead of $N = \infty$), and exact values of λ_p are computed from an $N \times N$ matrix equation (instead of approximate values from an approximate integro-differential equation). An important new result of the present computation is that, for the particular value $h^* = 0.262$, Flory's intrinsic viscosity function Φ is substantially independent of N in the range $50 \leq N \leq 300$ and has the value 2.85×10^{23} ml/g; this equals the value given by Zimm's original approximate calculation for the case $N = \infty$, $h \gg 1$. This suggests that the interpretation of intrinsic viscosity data in terms of the well-known 'non-tree-draining' concept should be reconsidered.

EXACT RELAXATION TIMES AND DYNAMIC FUNCTIONS FOR DILUTE POLYMER SOLUTIONS FROM THE BEAD/SPRING MODEL OF ROUSE AND ZIMM*

A. S. Lodge and Yeen-Jing Wu

1. Introduction

In the well-known theories of Rouse (1) and Zimm (2) for very dilute solutions of long-chain ('linear polymer') molecules, each polymer molecule is represented by N equal 'thermal motion' 'Gaussian' springs connected end-to-end; the solvent is treated as a constant-temperature environment for the polymer molecules and also as a Newtonian incompressible liquid, of viscosity η_s , which interacts with each polymer molecule only at $N + 1$ point centers ('beads') situated at the ends of the N springs. Each bead has the same 'friction constant' f_0 (which would be equal to $6\pi a \eta_s$ if the bead were a rigid sphere of radius a treated according to Stokes' law). Each spring has the same root-mean-square end-to-end distance b when the solution is not flowing.

Compared with earlier theories (3) in which equal friction constants were assigned to each atom on the 'backbone' of a polymer molecule, the bead/spring theory of Rouse and Zimm involves an extra artificial feature, namely, the concentration of polymer-solvent hydrodynamic interaction at the $N + 1$ fictitious beads. The advantages arising from the simpler mathematics involved, however, are considerable: the dynamic viscosity η' and dynamic rigidity G'

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as functions of angular frequency ω , for oscillatory small-amplitude shear, have been calculated (1, 2, 4) and compared rather extensively with experimental data (5); more recently, the (macroscopic) constitutive equations, from which all rheological properties in isothermal homogeneous flows can be calculated, have been derived by Lodge and Wu (6), who also list all the assumptions involved in the theory. Precise calculation of the dynamic functions $\eta'(\omega)$, $G'(\omega)$ has recently assumed added importance because improvements in experimental techniques have made possible the extrapolation to zero polymer concentration of the data obtained (7, 8); such 'intrinsic' data can thus properly be compared with the predictions of the bead/spring theory which is based on neglect of interactions between different polymer molecules.

In order to compute the functions $\eta'(\omega)$, $G'(\omega)$, it is necessary to compute the characteristic values λ_p ($p = 1, 2, \dots, N$) of the symmetric matrix $N \times N$ B [B_{pq}] whose elements B_{pq} are given by the equations

$$B_{pq} = H_{pq} + H_{p-1,q-1} - H_{p-1,q} - H_{p,q-1} \quad (p, q = 1, 2, \dots, N), \quad [1.1]$$

where

$$H_{ij} = \begin{cases} 1 & (i = j) \\ 2^{1/2} h^* |i-j|^{-1/2} & (i, j = 0, 1, 2, \dots, N), \\ & (i \neq j) \end{cases} \quad [1.2]$$

$$h^* = f_0 / [(12\pi^3)^{1/2} \eta_s b]. \quad [1.3]$$

The matrix B has been introduced by Lodge and Wu (6) as a more convenient alternative to Zimm's singular, non-symmetric, matrix HA which has the characteristic values $0, \lambda_1, \lambda_2, \dots, \lambda_N$ (6); $H = [H_{ij}]$, and A is defined in equation (11) of Zimm (2).

The object of the present paper is to present the results of computing 'exact' characteristic values $\lambda_1, \lambda_2, \dots, \lambda_N$ of the matrix B , together with various functions of the λ_p of interest for comparison with experimental data obtained in steady- and oscillatory-shear flow. Available computer storage facilities have enabled us to use values of N up to 300, which may well prove to be sufficient for the highest-molecular-weight polymers available. The only other published exact computations (for non-zero h^*) are those of Thurston and Morrison (9), whose restriction $N \leq 15$ is rather severe.

We call our values for λ_p 'exact' to distinguish between them and the approximate values obtained by Zimm, Roe, and Epstein (10), Hearst (11), and Tschoegl (4) (Table 1), who replaced the discrete eigenvalue problem (associated with matrix equations involving B or HA) by a discrete eigenvalue problem associated with an integro-differential equation (equation (71) of Zimm (2)) regarded as an approximation to the actual matrix equation given by the Zimm model. The approximation involved here has been thought to be reliable when N is large; recently, however, partly as a result of comparing our exact values for λ_p with those obtained from the Zimm integro-differential equation, Osaki (12) has noted that Zimm's equation is incorrectly derived from the matrix equation, and that the corrected equation is the following:

$$\alpha(r)(1 - 4h^*) + h \int_{-1}^1 \alpha''(s) |r - s|^{-1/2} ds = -N^2 \lambda \alpha(r)/4 . \quad [1.4]$$

Zimm's equation omits the term $-4h^* \alpha(r)$. Zimm's parameter h is given by the equation

$$h = h^* N^{1/2} . \quad [1.5]$$

In Table 1, the notation $h \gg 1$ (used by Zimm) means that, on the left-hand side of [1.4], the integral term alone is retained; as Osaki (12) has observed, this case really corresponds to the value $h^* = 0.25$ (and N large) when the correct approximate equation [1.4] is used.

TABLE 1: Calculations of characteristic values λ_p for the bead/spring theory of Rouse and Zimm

	N	h	h^*	
1. Rouse (1)	1 to ∞	0	0	exact
2. Zimm, Roe, and Epstein (10)	large	$\gg 1$		approximate
3. Hearst (11)	large	> 0		approximate
4. Tschoegl (4)	large	> 0		approximate
5. Thurston and Morrison (9)	1 to 15		0 to 0.4	exact
6. Wu (13)	1 to 222		0.05 to 0.3	exact
7. Lodge and Wu (this paper)	2 to 300		0.05 to 0.3	exact

In view of the idealization inherent in the bead/spring model and various approximations used in Zimm's analysis of this model (on which our

present calculations and all the calculations of Table I are based), it might be argued that the present computations amount to hair splitting; we recognize the weaknesses that remain, but consider that it is worth while making the present computations if only to eliminate any easily avoidable approximations in the analysis of the model and so render it more open to critical examination. Pyun and Fixman (14) have made certain calculations based on the bead/spring model without using one of Zimm's assumptions (namely, that the Oseen hydrodynamic interaction tensor can be replaced by its value averaged in the solution at rest); Wu (13) has compared results of Pyun and Fixman's calculations with the results of the present paper.

The characteristic values λ_p are dimensionless functions of the parameters N, h^* . Certain constants τ_p , called 'relaxation times', defined by the equations

$$\tau_p \lambda_p = (\pi^3/3)^{1/2} \eta_s b^3 h^*/(kT) \quad (p = 1, 2, \dots, N), \quad [1.6]$$

where k and T denote Boltzmann's constant and absolute temperature, play a fundamental role in the theory. The present report thus computes exact relaxation times in terms of three parameters, whose values are unknown a priori. The selection of these three parameters may be made in various ways, some of which are listed in Table 2.

TABLE 2. Selections of three basic parameters

1. N, f_0, b	N springs per molecule; $f_0 =$ bead friction constant; $b =$ r.m.s. spring length at rest;
2. N, h^*, b	$h^* = f_0 / [(12\pi^3)^{1/2} n_s b]$;
3. N, h^*, τ_1	$\tau_1 = f_0 b^2 / [6 kT \lambda_1(N, h^*)]$;
4. N, h, τ_1	$h = h^* N^{1/2}$;
5. N, h^*, τ_0	$\tau_0 = \sum_{p=1}^N \tau_p$;
6. m_1, h^*, b	$m_1 = M/N$ (M = polymer molecular weight).

We follow the usual notation according to which $\lambda_1 < \lambda_2 < \dots < \lambda_N$. λ_1 is thus the smallest characteristic value, and hence τ_1 is the greatest relaxation time.

2. Computation of $\lambda_1, \lambda_2, \dots, \lambda_N$.

$\lambda_1, \lambda_2, \dots, \lambda_N$ are the roots in λ of the equation

$$\det(B_{pq} - \lambda \delta_{pq}) = 0. \quad [3.1]$$

When $h^* = 0$, the roots are given by the equations

$$\lambda_p = 4 \sin^2 [p\pi/2(N+1)] \quad (p = 1, 2, \dots, N) \quad [3.2]$$

given by Rouse (1). When $h^* \neq 0$, the roots for the cases $N = 1, 2$ are as follows:

$$\lambda_1 = 2(1 - 2^{1/2} h^*) \quad (N = 1) :$$

[3.3]

$$\lambda_1 = 1 - h^*, \quad \lambda_2 = 3 + (1 - 2^{1/2}) h^* \quad (N = 2).$$

For $h^* \neq 0$ and $N > 3$, we know of no method of obtaining a solution for the λ_p in closed form. To obtain solutions by numerical methods, a Fortran program was written in order to compute roots of [3.1] by means of a combination of Householder's method and the 'Q-R method'; the University of Wisconsin-Madison Computing Center's UNIVAC 1108 and 'BUMP 2' Library Subroutine were used; in this way, values of $\lambda_1, \lambda_2, \dots, \lambda_N$ were obtained for various values of h^* and for values of N up to 222 (13); computer storage limitations made it impossible to handle higher values of N using this program. Subsequently, use was made of the fact that B is symmetric, and a modified Miami University Program (H. J. Wertz version, dated 4/5/68) for handling packed matrices enabled the computations to be extended up to values of $N = 300$. To compute a complete set of characteristic values for a given value of N and a given value of h^* , the following times were required:

N:	25	50	100	200	300
Time in seconds:	0.3	1.6	10	70	235.

These times do not vary much with h^* .

Table 3 contains the results of computing various functions of the λ_p . The values of λ_1 and λ_N are tabulated. Values of $\lambda_2, \lambda_3, \dots, \lambda_{N-1}$ have not been tabulated here, but are available on request to one of the authors (A. S. L.); some have been tabulated by Wu (13).

The following checks on the computation confirm the reliability of the results and indicate that the computational error in Table 3 entries should nowhere exceed unity in the fourth significant figure:

1. Values obtained for λ_p are consistent with the equation

$$\sum_{p=1}^N \lambda_p = \text{Trace } B; \quad [3.1]$$

2. For $N = 1, 2, \dots, 15$, and various values of h^* , the values obtained for λ_p agree with those computed by Thurston and Morrison (9);
3. For $N = 1, 2$, values of λ_p are consistent with [3.3];
4. For $N = 50, 100, 200$ and $h^* = 0.1, 0.2, 0.3$, most of the tabulated functions were computed using both programs referred to above; comparison of entries showed agreement to three significant figures and, in most cases examined, to four significant figures; a few entries showed differences of unity in the fourth significant figure.

A minor advantage in using h^* , rather than h , as a parameter in the tabulation is that h^* has an upper limit, while h does not (assuming that N could be indefinitely great). We have chosen values of h^* in the interval $0.05 \leq h^* \leq 0.3$. Thurston and Morrison (9) quote the value 0.471 for the upper bound of h^* , but do not give details of their derivation; in an attempt to follow their argument, we obtain the value 0.65. Alternatively, using the very crude argument that $f_0 = 6\pi a\eta_s$ for a rigid spherical bead of radius a , the inequality $2a < b$ yields the result $h^* < 0.49$. Because of

the artificiality inherent in the model, we do not place much weight on the actual value of the upper bound on h^* given by such arguments; it seems reasonable, however, to suppose that there is an upper bound. Independent arguments based on a comparison of the results of the present calculations with measured data on intrinsic viscosity of polymer solutions suggest that the useful range for h^* is $0 < h^* \leq 0.26$. This range is fairly well covered by the entries in Table 3. Thurston and Morrison (9) have noted that the condition $h^* < 0.65$ is sufficient to ensure that λ_p shall be positive for $N = 1, 2$ (cf. [3.3]).

3. Steady shear flow functions

In the usual notation, we express the intrinsic viscosity $[\eta]$ in the form

$$[\eta] := \lim_{c \rightarrow 0} \frac{\eta - \eta_s}{c\eta_s} = \Phi \langle r^2 \rangle^{3/2} M^{-1} \quad [3.1]^{**}$$

where c is the polymer concentration in g/ml, η is the solution viscosity, and $\langle r^2 \rangle$ is the mean square end-to-end distance of a polymer molecule in the solution at rest. This equation may be regarded as a definition of the quantity Φ . The bead/spring theory gives the following equation for $\Phi = \Phi(N, h^*)$:

$$\Phi = (\pi^3 / 3)^{1/2} N_a h^* N^{-3/2} \sum_{p=1}^N \lambda_p^{-1}, \quad [3.2]$$

where $N_a = 6.0228 \times 10^{23}$ (Avogadro's number).

^{**}The notation $A := B$ means "A is defined by the equation $A = B$ ".

In Table 3, values of Φ are tabulated for various values of N and h^* . For comparison with the approximate values calculated by Tschoegl for $N = \infty$, the values of Φ have been plotted as functions of $\log h$ in Figure 1. It is seen that the experimentally-interesting range of values for Φ , namely $2.5 \leq 10^{-23}\Phi \leq 2.9$, are obtained with values of N in the range $25 \leq N \leq 300$ and values of h^* near 0.25, when the exact characteristic values are used, and with large values of h when the approximate characteristic values (with $N = \infty$) are used. In particular, for the special value $h^* = 0.262$, Table 3 gives the following values for Φ (in g/ml):

$N:$	8	25	50	100	200	300	[3.3]
$10^{-23}\Phi:$	2.954	2.864	2.853	2.852	2.855	2.856	($h^* = 0.262$)

For $25 \leq N \leq 300$, it is seen that $\Phi(N, h^*)$ (with $h^* = 0.262$) is substantially independent of N and that its value is close to the value 2.84×10^{23} obtained by Zimm (2) from the approximate calculation based on the values $N = \infty$, $h \gg 1$.

The case $h \gg 1$ is described by Zimm (2) as the "non-free-draining case", presumably because a large value of h is associated with a predominating bead-bead hydrodynamic interaction term in the equations of motion for a bead/spring unit and this in turn is believed to imply that, within a surface enveloping the polymer molecule, there is a substantial region of solvent which is 'immobilized' by the polymer molecule in the sense that the solvent velocity

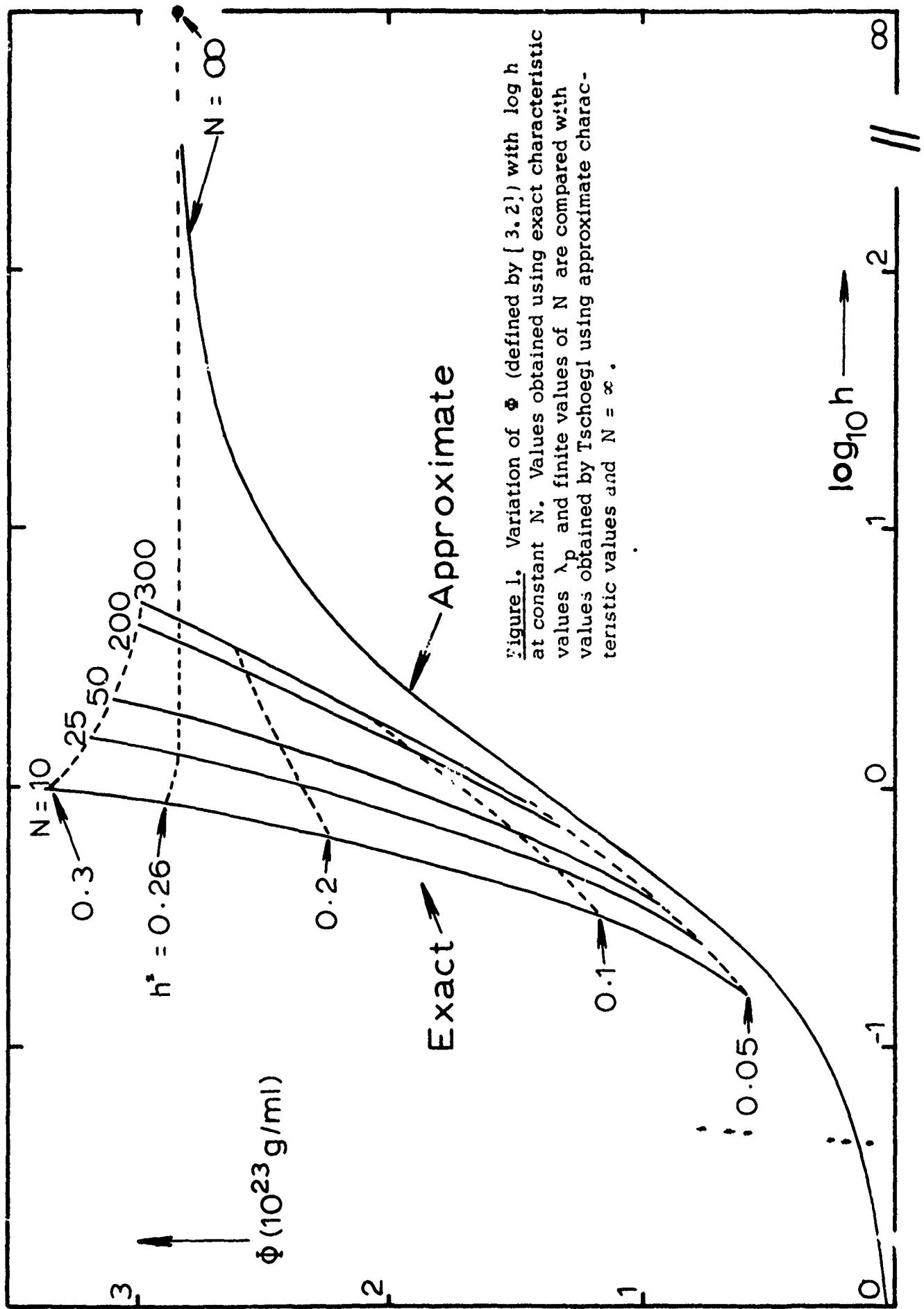


Figure 1. Variation of Φ (defined by [3, 2]) with $\log h$ at constant N . Values obtained using exact characteristic values λ_p and finite values of N are compared with values obtained by Tschoegl using approximate characteristic values and $N = \infty$.

equals some average polymer molecule velocity. Whether or not this concept could be substantiated for the case $h \gg 1$ by calculation of solvent and polymer velocities using the equations of the Zimm theory, our present results suggest that the concept of the non-free-draining limit may not in fact be appropriate for dilute solutions of linear polymers for which Φ has a value near 2.85×10^{23} g/ml: using our exact characteristic values, such a value is obtained when $h^* = 0.262$, and there seems to be no a priori reason for thinking that this value of the dimensionless friction constant is so large that partial or complete 'solvent immobilization' should occur.

In Figure 2, the data are replotted to show the variation of $\log \Phi$ with h^* at constant N ; the fact that the curves for $N \geq 25$ pass approximately through a common point (whose abscissa is 0.262) reflects the results [3.3].

For comparison of the theory with the experimentally determined molecular weight dependence of the intrinsic viscosity, Thurston and Morrison (9) make the reasonable assumption that N is proportional to M . For limited ranges of M values, both $[\eta]$ and $\langle r^2 \rangle$ (determined from light-scattering data) vary approximately as powers of M . In this connection, it is of interest to note that, according to our calculations, Φ can be represented approximately by an equation of the form

$$\Phi(N, h^*) = a_1(h^*) N^{n_1(h^*)} \quad [3.4]$$

for limited ranges of values of N ; the dependence of the index n_1 on h^* is shown in Figure 3: the fact that two curves are given for different ranges of

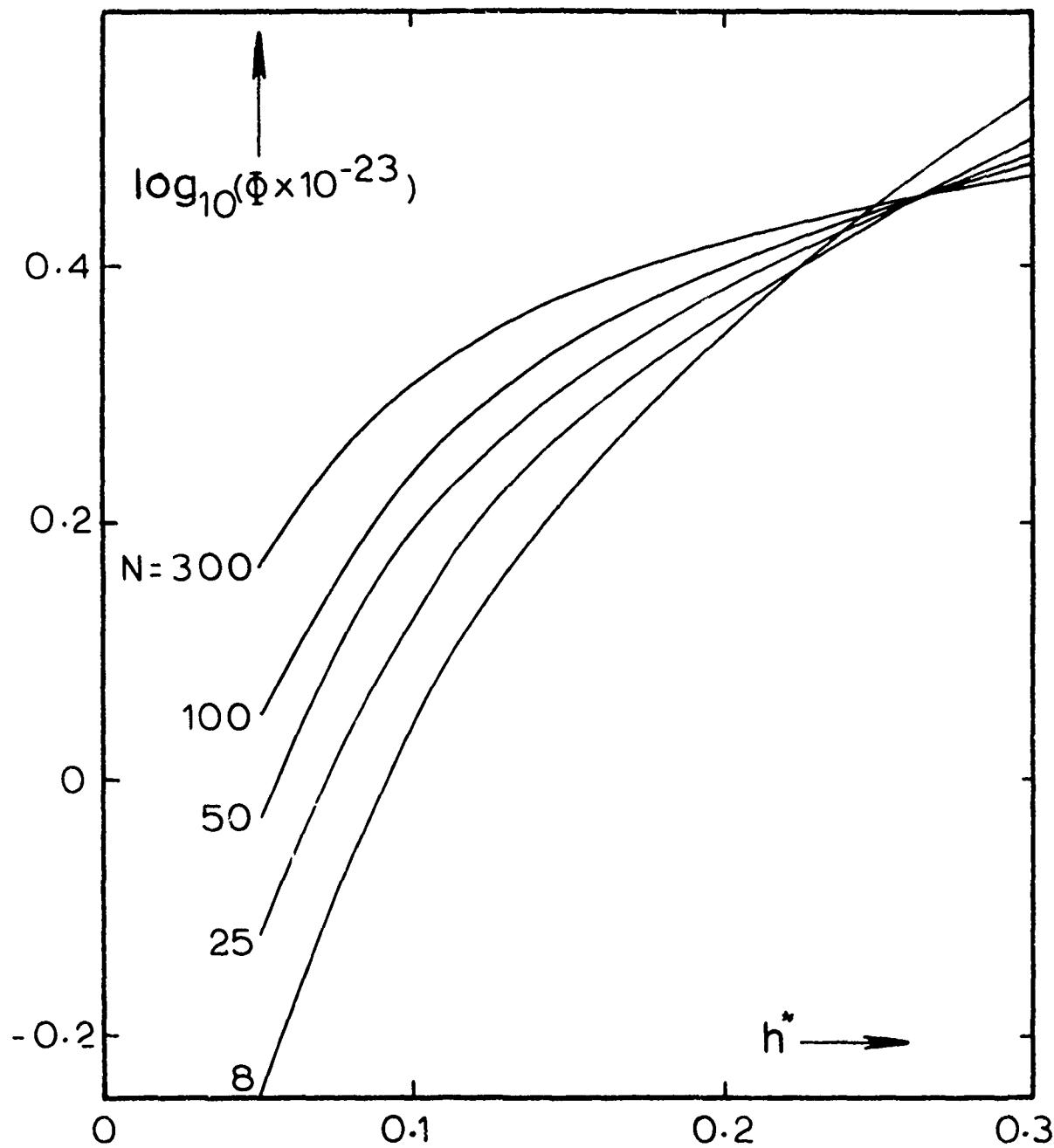


Figure 2. Variation of $\log \Phi$ with h^* at constant N calculated from [3.2] using exact characteristic values λ_p .

N reflects the fact that [3.4] is only an approximate representation of the dependence of Φ on N . Again, the fact that $n_1 = 0$ when $h^* = 0.262$ is a reflection of [3.3].

In Figures 4, 5, the quantities

$$\tau_0/\tau_1 \sum_{p=1}^N \tau_p/\tau_1 = \sum_{p=1}^N \lambda_1/\lambda_p, \quad [3.4]$$

$$J_{eR} = \frac{\sum_{p=1}^N \tau_p^2}{\left(\sum_{p=1}^N \tau_p \right)^2} = \frac{\sum_{p=1}^N \lambda_p^{-2}}{\left(\sum_{p=1}^N \lambda_p^{-1} \right)^2}, \quad [3.6]$$

are represented as functions of $\log h$ at constant values of N , and are compared with the corresponding quantities evaluated by Tschoegl (for $N \rightarrow \infty$) using approximate characteristic values.

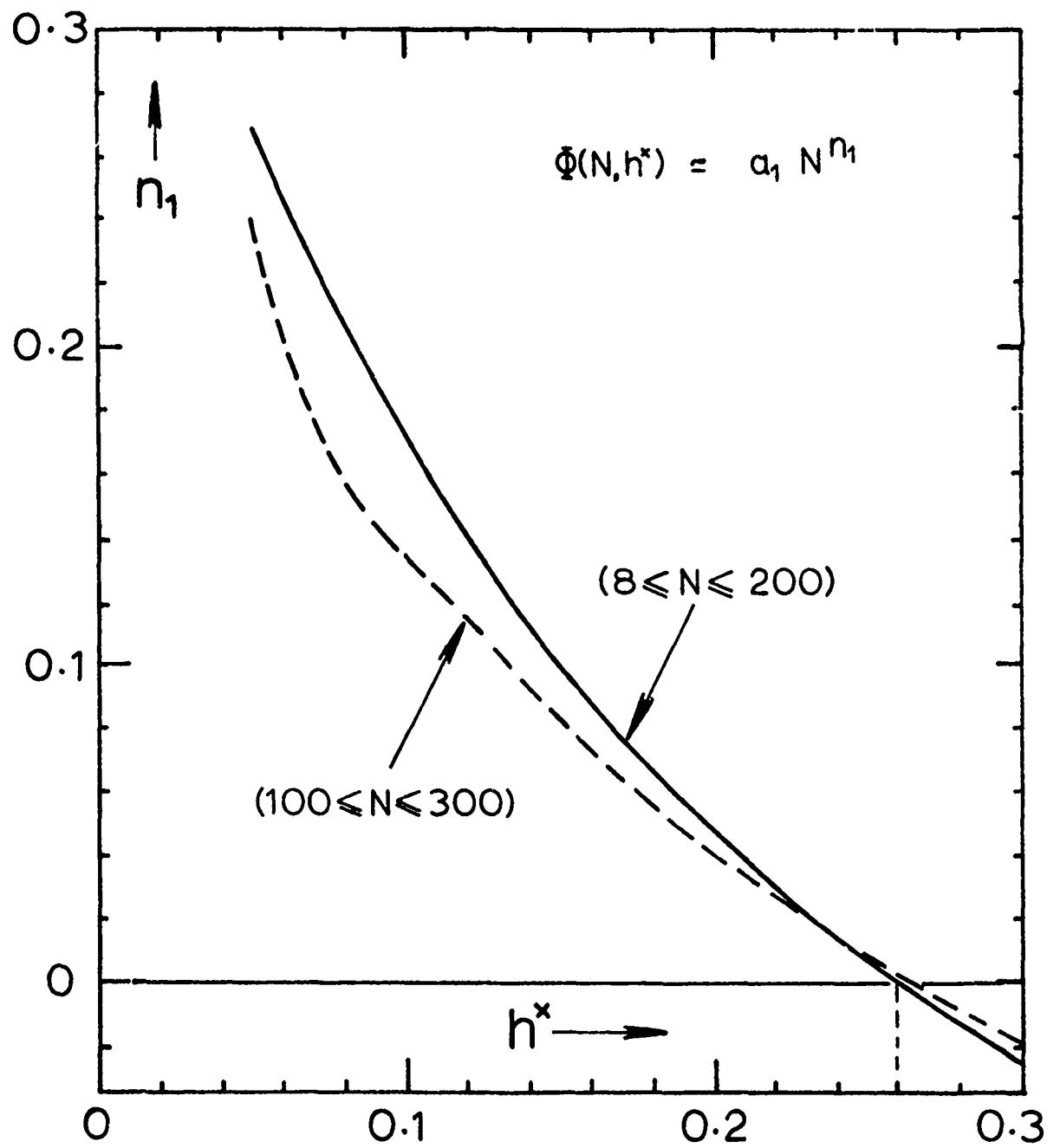


Figure 3. Dependence of index n_1 on h^* , where $\Phi(N, h^*)$, calculated from [3.2] using exact characteristic values λ_p , is represented approximately by [3.4].

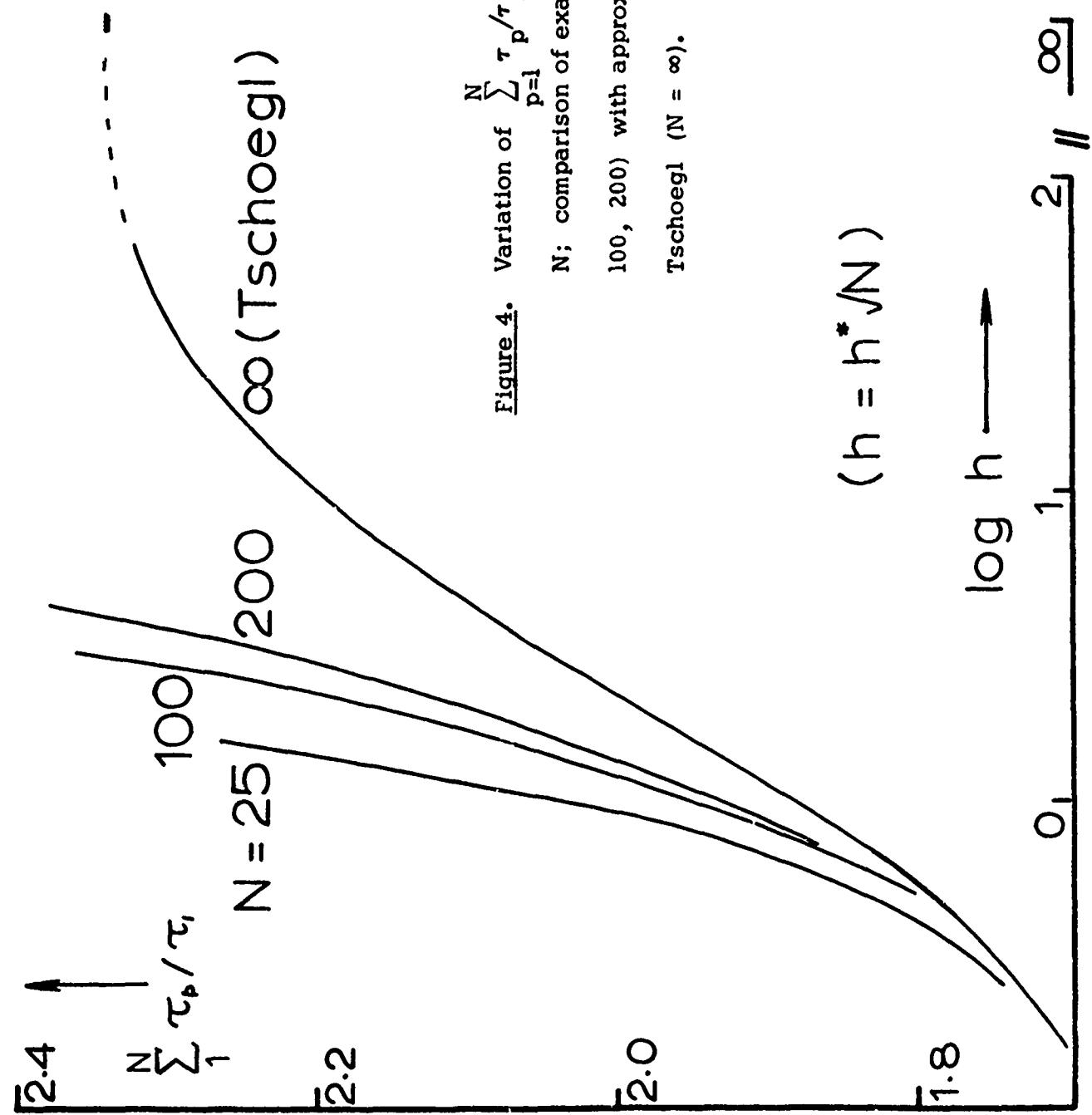
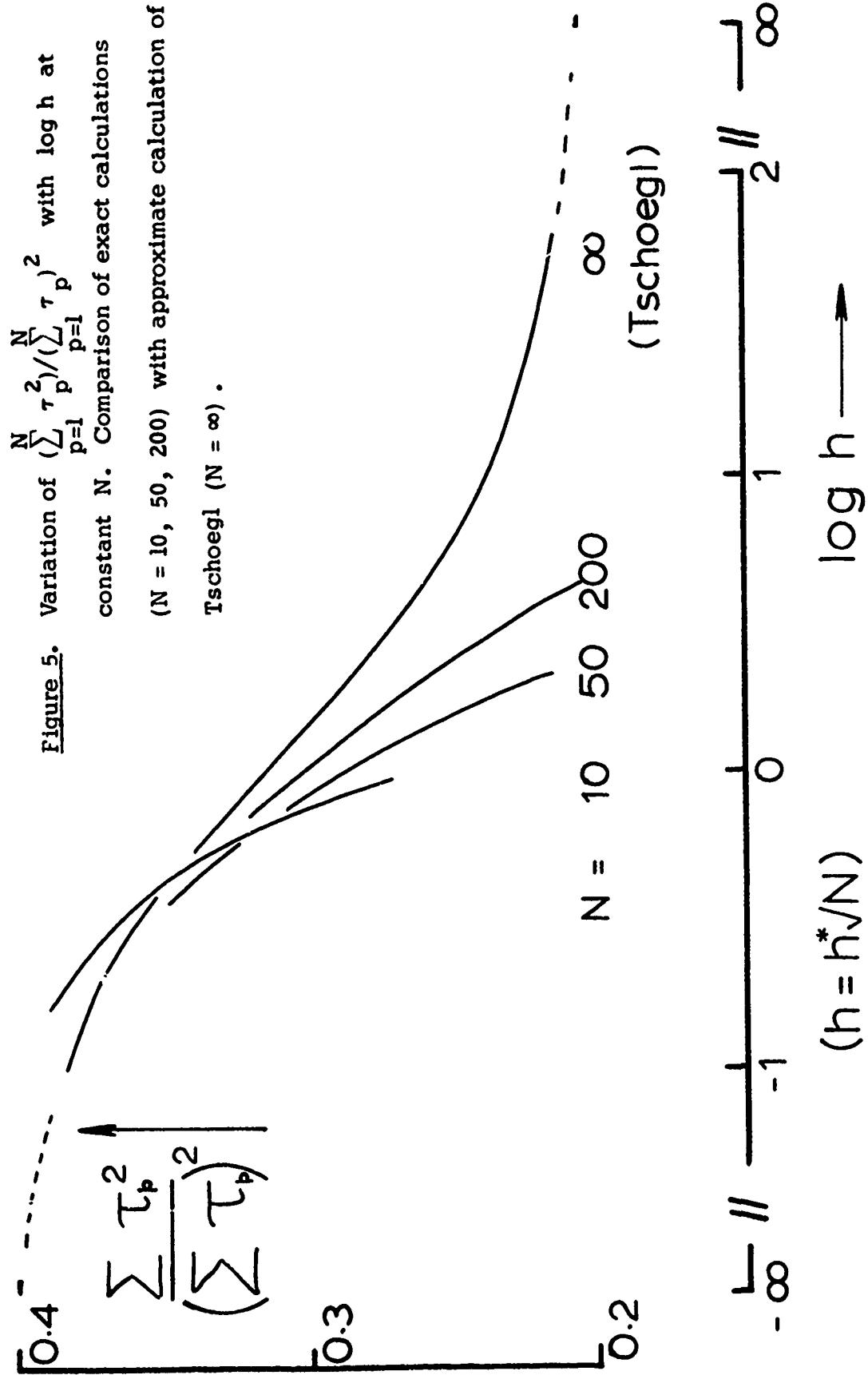


Figure 4. Variation of $\sum_{p=1}^N \tau_p / \tau_1$ with $\log h$ at constant N ; comparison of exact calculations ($N = 25, 100, 200$) with approximate calculations of Tschoegl ($N = \infty$).



4. Small-strain oscillatory shear

According to the bead/spring theory (2), the dynamic viscosity η' and dynamic rigidity G' in a state of steady sinusoidal oscillatory shear of small strain amplitude satisfy the equations

$$\lim_{c \rightarrow 0} \frac{\eta' - \eta_s}{c} = \frac{RT}{M} \tau_1 \eta'_R(N, h^*, \omega\tau_1), \quad [4.1]$$

$$\lim_{c \rightarrow 0} \frac{G'}{c\omega} = \frac{RT}{M} \tau_1 \eta''_R(N, h^*, \omega\tau_1), \quad [4.2]$$

where $R = kN_a$,

$$\eta'_R := \sum_{p=1}^N \frac{\lambda_1}{\lambda_p} \left\{ 1 + \left(\omega\tau_1 \frac{\lambda_1}{\lambda_p} \right)^2 \right\}^{-1}, \quad [4.3]$$

$$\eta''_R := \omega\tau_1 \sum_{p=1}^N \left(\frac{\lambda_1}{\lambda_p} \right)^2 \left\{ 1 + \left(\omega\tau_1 \frac{\lambda_1}{\lambda_p} \right)^2 \right\}^{-1}, \quad [4.4]$$

and ω denotes the angular frequency. The greatest relaxation time τ_1 , according to [1.6], is given by the equation

$$\tau_1 = \tau_1(N, h^*, b) = \left(\frac{\pi^3}{3} \right)^{1/2} \frac{\eta_s}{kT} \frac{b^3 h^*}{\lambda_1(N, h^*)}, \quad [4.5]$$

and is thus a function of the three parameters N, h^*, b .

Using the exact characteristic values, the functions $\eta'_R(N, h^*, \omega\tau_1)$ and $\eta''_R(N, h^*, \omega\tau_1)$ have been computed for values of N, h^* , and $\log_{10}\omega\tau_1$ in ranges of practical interest. The results, together with values of related functions of interest, are given in Table 3.

In figures 6-9, $\log \eta'_R$ and $\log \eta''_R$ are plotted as functions of $\log \omega\tau_0$, where τ_0 is defined by the equation

$$\tau_0 := \sum_{p=1}^N \tau_p . \quad [4.6]$$

τ_0 is a convenient dimensionless variable to choose for the abscissa when comparing dynamic functions η'_R and η''_R obtained using different values of parameters N , h^* and different methods of calculation (exact and approximate): from [4.1], [4.3] and the fact that $\eta = \eta'$ when $\omega = 0$, it follows that

$$[\eta] = \frac{RT}{M\eta_s} \tau_0 . \quad [4.7]$$

Comparison of curves using the abscissa $\log \omega \tau_0$ thus amounts to comparison at constant $[\eta]$.

From Figure 6, it is seen that there is a small but significant difference between the exact and the approximate curves when $h = 2$; the differences at the largest values of $\log \omega \tau_0$ doubtless reflect the difference in values of N ($100, \infty$) used in the comparison (see also Figure 7); the difference in curves at lower frequencies is attributed to errors arising in the approximate calculation (based on the use of [1.4] without the term $-4h^* \alpha(r)$).

From Figure 7, it is seen that, when $h^* = 0.3$, a change in the value of N from 50 to 200 leaves the low-frequency behavior substantially unaltered but moves the point of intersection of the η'_R -curve and the η''_R -curve to higher frequencies.

Figures 8 and 9 compare the Zimm curves ($N = \infty, h \gg 1$) with the exact curves for high ($h^* \approx 0.3$) and low ($h^* = 0.1$) values of the friction constant.

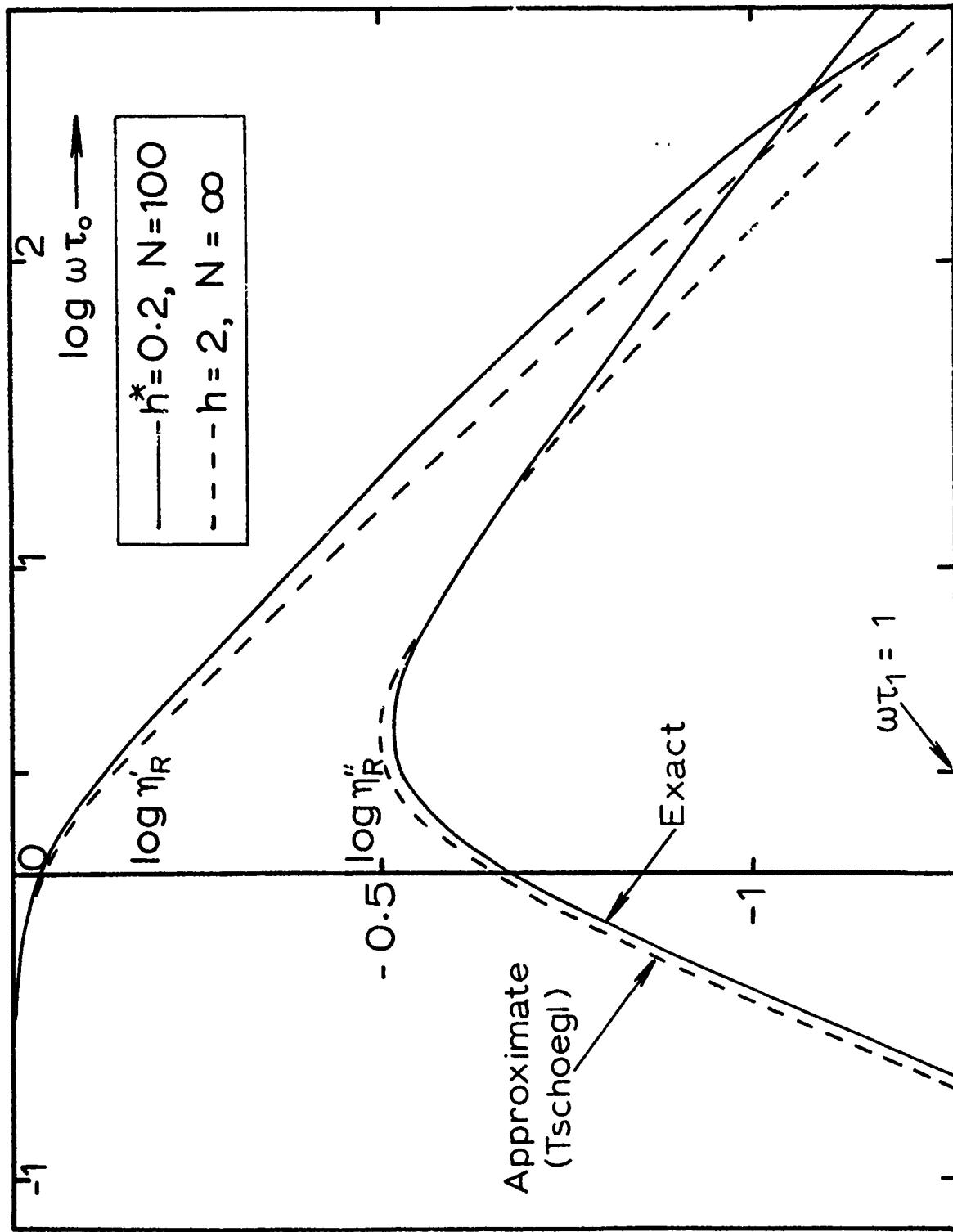


Figure 6. Reduced dynamic functions versus frequency. Comparison of exact calculation ($N = \infty$) with approximate calculation ($N = 100$) for the case $h = 2$.

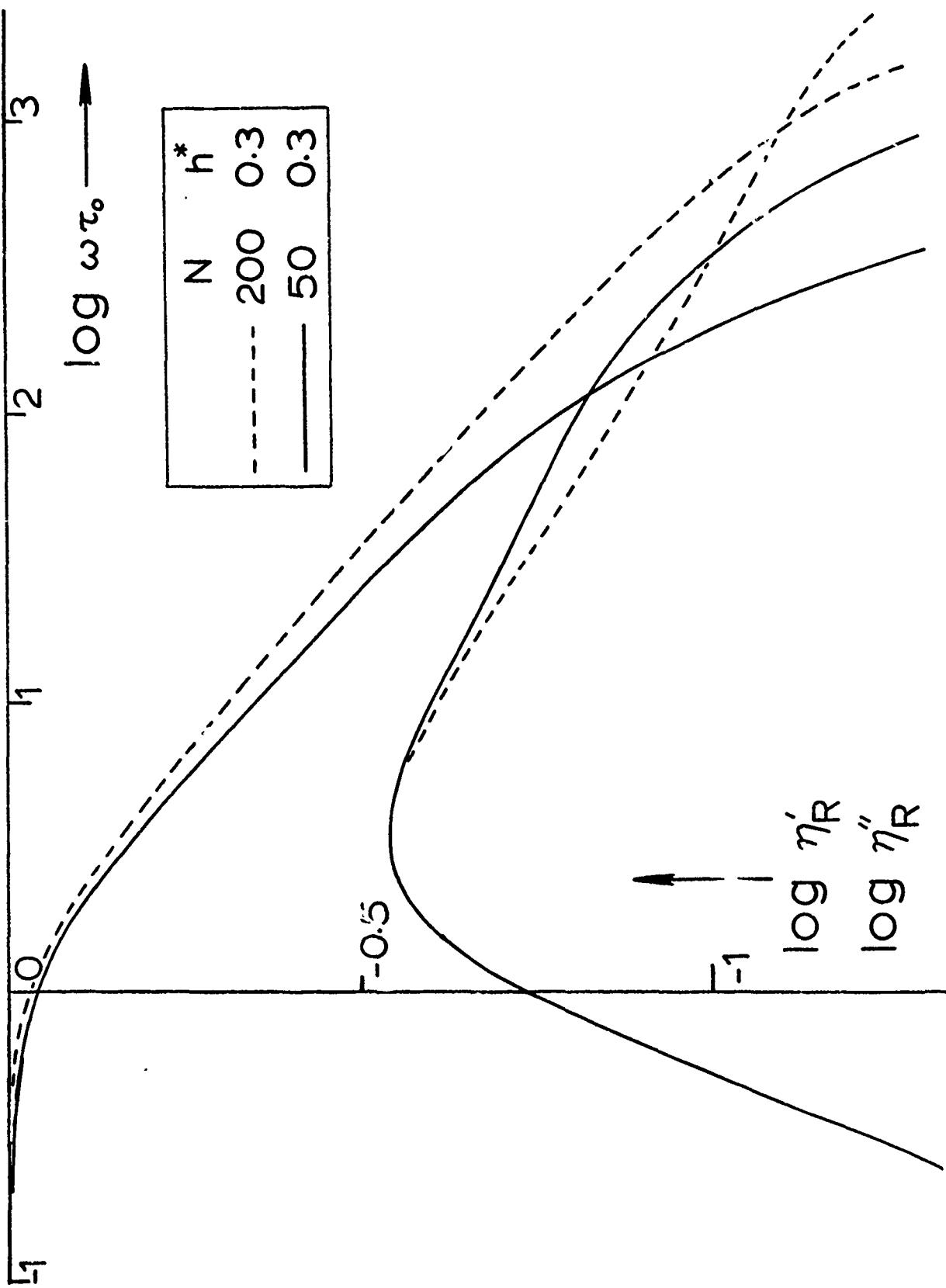


Figure 7. Reduced dynamic functions versus frequency (exact calculations). * Comparison of $N = 50$ and $N = 200$ for the case $h^* = 0.3$.

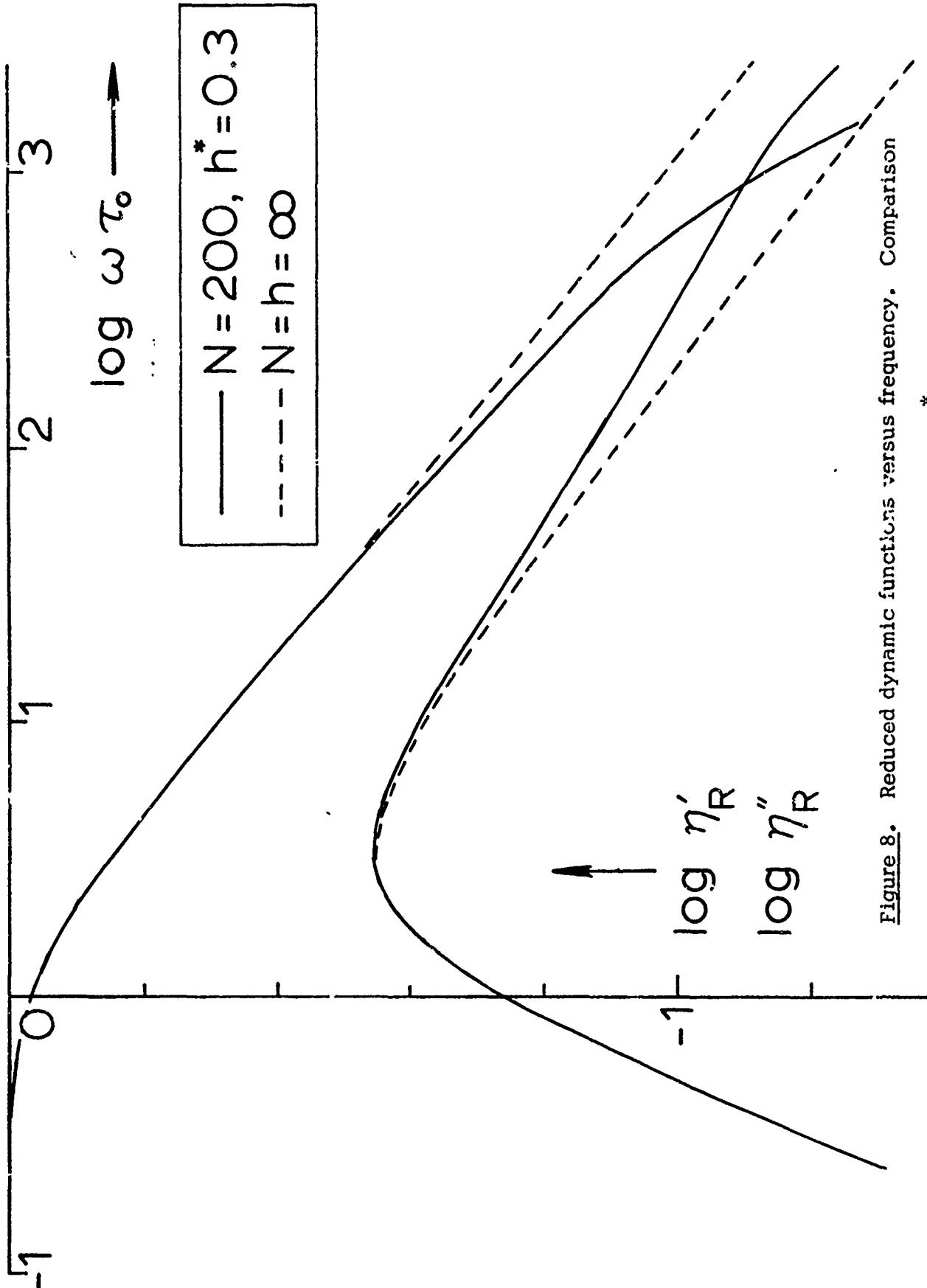


Figure 8. Reduced dynamic functions versus frequency. Comparison
 of exact calculations ($N = 200$, $h^* = 0.3$) with approximate
 calculations ($N = \infty$, $h \gg 1$) of Zimm.

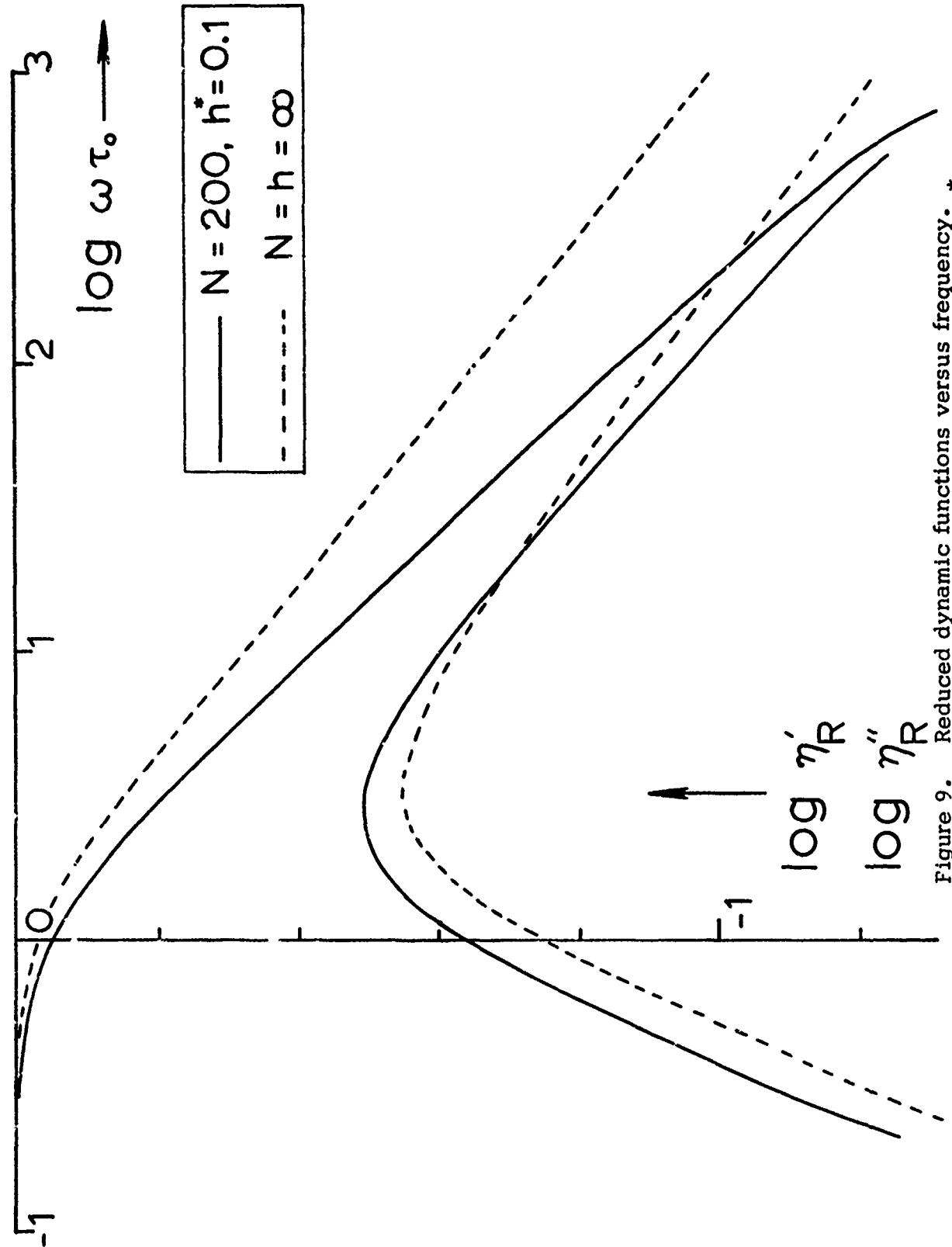


Figure 9. Reduced dynamic functions versus frequency.
Comparison of exact calculations ($N = 200, h^* = 0.1$)
with approximate calculations ($N = \infty, h \gg 1$) of Zimm.

It is intended, in a future publication, to present results of a comparison of the present calculations with experimental data giving the variation of $[\eta]$ with M and of η' and G' with ω .

5. Discussion

The present calculations are simply an extension of the calculations of Thurston and Morrison (9) to values of N up to 300. In comparison with the earlier calculations of Zimm and Tschoegl, the importance of our calculations and those of Thurston and Morrison is twofold: (i) our calculations are exact (within the confines of the Zimm treatment of the bead/spring model); and (ii) N , the number of springs per polymer molecule, appears as an additional parameter whose value is at our disposal when we wish to compare theoretical predictions with experimental data on any given solution of linear polymer molecules of equal molecular weight.

It is possible that (ii) is more important, and more open to question, than (i). Thurston and Morrison (9) have already made use of (ii) in offering a possible interpretation of the dependence of $[\eta]$ on M , using the assumption that N is proportional to M for a given polymer/solvent system. Thurston and Schrag (15) have similarly interpreted their experimental data on oscillatory flow birefringence; for values of M down to 10^3 , they use values of N down to 1 for the polystyrene/Aroclors system.

We do not propose here to embark on a comprehensive discussion of the issues raised by the use of N as a parameter, but we do recognize that

this use is open to the criticism that N is too closely connected with the main artificial feature of the bead/spring model (namely, the arbitrary concentration of hydrodynamic interaction at discrete points on the Gaussian spring system) to provide a meaningful parameter having significance for any actual polymer solution. Awareness of this criticism no doubt influenced the early applications of the bead/spring theory (1, 2, 4, 5) in which the equations were cast in a form in which N did not appear: this was achieved partly taking $N = \infty$ in the upper limits of sums in equations such as [3.2], [3.4], and [3.6] and partly by the use of the integro-differential eigenvalue equation for the case of very large N . On the other hand, the use of very large values of N is itself open to criticism: for a given polymer molecule, a certain minimum number (perhaps not well-defined, but nonetheless real) of backbone bonds are required in order that the corresponding part of the molecule may be approximately treated as a Gaussian spring; furthermore, the fact that N may not appear in an equation does not, by itself, eliminate the dependence of the equation on the artificial feature of the model.

We are perhaps on safer ground if we confine applications of the bead/spring theory to properties for which the results predicted by the theory are insensitive to the value of N ; an example is furnished by the low-frequency behavior of the dynamic functions shown in Figure 7. On the other hand, it is just conceivable that a more fundamental treatment of polymer/solvent dynamics than that represented by the bead/spring idealization could furnish criteria for the validity of the bead/spring idealization (with finite N).

as an approximation. We hope that the calculation of the present report, when compared critically with suitable experimental data, might lead to a better understanding of the justification for and limitations of the bead/spring model.

Acknowledgments

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Table 3: Exact characteristic values and steady-and oscillatory-shear-flow functions

Key to entries

L1	LN	1/(LN)	SUM 1/(LP)	SUM LI/LP	RECIP ROCAL	SUM (1/LP)2	SUM(L1 /LP)2	JER	PHI
λ_1	λ_N	λ_N^{-1}	$\sum_1^N \lambda_p^{-1}$	$\sum_1^N \frac{\lambda_1}{\lambda_p}$	$(\sum_1^N \frac{\lambda_1}{\lambda_p})^{-1}$	$\sum_1^N \frac{1}{\lambda_p^2}$	$\sum_1^N (\frac{\lambda_1}{\lambda_p})^2$	J_{eR}	$\Phi \times 10^{-23} g/ml$

[3.1]

[3.6] [3.2]

LOG	OMTI	ETAIR	ETA2R	G1R	G2R	MOD	ARCTAN	H*
\log_{10}	$\omega\tau_1$	η'_R	η''_R	G'_R	G''_R	$ \eta'_R + i\eta''_R $	$\tan^{-1} \frac{\eta''_R}{\eta'_R}$	h^*

[4.3] [4.4] $\omega\tau_1 \eta''_R$ $\omega\tau_1 \eta'_R$

Exponential notation: .769-03 means 0.769×10^{-3} .

Parameter values

h^*	0.05	0.075	0.1	0.13	0.15	0.2	0.25	0.262	0.3
N									
2	X			X	X		X		
4	X	X		X	X	X	X		
8	X	X	X	X	X	X	X	X	
25	X	X	X	X	X	X	X	X	X
50	X	X	X	X	X	X	X	X	X
100	X	X	X	X	X	X	X	X	X
200	X	X	X	X	X	X	X	X	X
300	X	X	X	X	X	X	X	X	X

EXACT ZIMM EIGENVALUES
 $L_1 \quad LN \quad I/(LN)$ $SUM \quad 1/(LP)$
 L_1/LP RECIP $SUM(L_1) \quad 1/(LP)$
 R_{OCAL} $(1/(LP))^2 \quad (LP)^2$
 $I/(LP)^2$ JFR
 $N = 2 \quad H = .075$
 P_H
 -23
 $.13349 \quad .741$
 $.13349 \quad 1.1218$
 $.616$
 $.745$

MOULDS AND VISCOSITY OF POLYAMIDE WISECOSEITY

EXACT ZINN EIGENVALUES

EXACT ZIMM EIGENVALUES		$N = 2$		$N = 130$	
L_1	$\ln L_1 / \ln N$	SUM	RECIP	SUM	SUM
-870+00	-239+01	-418+00	-157+01	(1/LP) ²	(1/LP) ²
-870-00	-239-01	-418-00	-157-01	1.1/LP	1.1/LP
-870+00	-239+01	-418+00	-157+01	1.363	734
-870-00	-239-01	-418-00	-157-01	-1.363	-734
-870+00	-239+01	-418+00	-157+01	-150+01	-150+01
-870-00	-239-01	-418-00	-157-01	1.1320	1.1320
-870+00	-239+01	-418+00	-157+01	-609	-609
-870-00	-239-01	-418-00	-157-01	1.395	1.395
-870+00	-239+01	-418+00	-157+01	-23	-23
-870-00	-239-01	-418-00	-157-01	PHI	PHI

BREVILIS ET VITIOSITATE UND MUTH

EXACT ZIMM EIGENVALUES
LI LN I / LN) • 435.00
• 850.00 • 230.01

$$\begin{aligned} \text{N} &= 2 \sum_{i=1}^{15} H_i = 150 \\ \text{SUN} &= 11 / 12 \\ \text{MOON} &= 1 / 12 \\ \text{TUE} &= 1 / 12 \\ \text{WED} &= 1 / 12 \\ \text{THU} &= 1 / 12 \\ \text{FRI} &= 1 / 12 \\ \text{SAT} &= 1 / 12 \end{aligned}$$

REDUCED DYNAMIC VISCOSITY AND MODULUS

EXACT ZIMM EIGENVALUES
 L1 LNN 1/(LN)
 1/(LP) SUM RECIP SUM RECIP
 .750+00 184+01 545+00 188+01 1.409 710 (1/LP)2 (LP)2
 .207+01 1.1669 .588 3.214

N= 2 H= 250
 SUM SUM(L1) JFR PHI
 (1/LP)2 (LP)2 -23
 .207+01 1.1669 .588 3.214

REDUCED DYNAMIC VISCOSITY AND MODULUS

L1	LNN	1/(LN)	SUM	RECIP	SUM	SUM(L1)	JFR	PHI	M00	ARCTAN
LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	E1A2/1	
0MT1	FTAIR	ETA2R	G1R	G2R	ETAIR	ETA2R	G1R	G2R	E1A2/1	
-2.8	-149	-2.733	-5.533	-2.651	-161+01	-185-02	-293-05	-223-02	-141+01	-131-C2
-2.0	-149	-1.933	-3.933	-1.851	-141+01	-117-01	-117-03	-141-01	-141+01	-828-02
-1.8	-149	-1.733	-3.533	-1.651	-141+01	-185-01	-293-03	-223-01	-141+01	-131-C1
-1.4	-148	-1.334	-2.734	-1.252	-141+01	-464-01	-185-02	-560-01	-141+01	-330-01
-1.0	-145	-0.937	-1.937	-0.855	-140+01	-116+00	-116-01	-140+00	-140+01	-826-01
-0.8	-141	-0.742	-1.542	-0.659	-138+01	-181+00	-287-01	-219+00	-139+01	-130+00
-0.6	-129	-0.556	-1.156	-0.471	-134+01	-278+00	-698-01	-338+00	-137+01	-204+00
-0.4	-101	-0.389	-0.789	-0.299	-126+01	-408+00	-163+00	-502+00	-133+01	-313+00
-0.2	-041	-0.260	-0.450	-0.159	-110+01	-550+00	-347+00	-693+00	-123+01	-464+00
0.0	-071	-0.192	-0.192	-0.071	-850+00	-643+00	-643+00	-850+00	-107+01	-648+00
0.2	-242	-0.195	-0.075	-0.042	-573+00	-638+00	-101+01	-908+00	-857+00	-839+00
0.4	-474	-0.261	-0.139	-0.074	-336+00	-548+00	-138+01	-842+00	-642+00	-102+01
0.6	-766	-0.378	-0.222	-0.165	-171+00	-419+00	-167+01	-682+00	-452+00	-118+01
0.8	-108	-0.534	-0.265	-0.318	-779-01	-292+00	-184+01	-492+00	-303+00	-131+01
1.0	-1482	-0.714	-0.286	-0.482	-330-01	-193+00	-193+01	-330+00	-196+00	-140+01
1.2	-1870	-0.905	-0.295	-0.670	-135-01	-124+00	-197+01	-214+00	-125+00	-146+01
1.4	-2266	-1.101	-0.299	-0.866	-543-02	-792-01	-199+01	-356+00	-764-01	-150+01
1.6	-2.654	-1.300	-0.300	-1.064	-217-02	-501-01	-203+01	-502-01	-153+01	-156+01
1.8	-3.063	-1.493	-0.301	-1.263	-865-03	-317-01	-200+01	-546-01	-317-01	-154+01
2.0	-3.463	-1.699	-0.301	-1.463	-345-03	-200-01	-200+01	-345-01	-200-01	-155+01
2.2	-3.863	-1.899	-0.301	-1.663	-177-03	-126-01	-200+01	-303+00	-131+01	-156+01
2.4	-4.262	-2.099	-0.301	-1.862	-546-04	-796-02	-200+01	-137-01	-796-02	-156+01
2.6	-4.662	-2.299	-0.301	-2.062	-218-04	-502-02	-200+01	-866-02	-502-02	-157+01
2.8	-5.062	-2.499	-0.301	-2.262	-866-05	-317-02	-200+01	-546-02	-317-02	-157+01
3.0	-5.462	-2.699	-0.301	-2.462	-345-06	-200-02	-200+01	-345-02	-200-02	-157+01
3.4	-6.262	-3.099	-0.301	-2.862	-546-06	-796-03	-200+01	-137-02	-796-03	-157+01
3.8	-7.062	-3.499	-0.301	-3.262	-866-07	-317-03	-200+01	-546-03	-317-03	-157+01
4.2	-7.862	-3.899	-0.301	-3.662	-137-07	-126-03	-200+01	-218-03	-126-03	-157+01
4.6	-8.662	-4.299	-0.301	-4.062	-218-08	-502-04	-200+01	-866-04	-502-04	-157+01
5.0	-9.462	-4.699	-0.301	-4.462	-345-09	-200-04	-200+01	-345-04	-200-04	-157+01

EXACT ZIMM EIGENVALUES
 L_1 L_N $1/(LN)$
 $0.372410 \cdot 302401 \cdot 331400$

EXACT ZIMM EIGENVALUES
 $L_1 \quad \ln \quad 1/(LN)$
 $L_2 \quad 1/(LP) \quad 1/(LP)$
 $L_3 \quad 1/(LP) \quad 1/(LP)$
 $L_4 \quad 1/(LP) \quad 1/(LP)$

REDUCED DYNAMIC VISCOSITY AND MOULDS

	LOG	LOG	LOG	OMT1	ETA1R	ETA2R	G1Q	G2P	LOG	LOG	ETA1P	ETA2R
-2.8	• 201	-2.746	-5.546	-2.599	-159+01	• 190-02						
-2.0	• 201	-1.946	-3.946	-1.799	-159+01	• 113-01						
-1.8	• 201	-1.746	-3.546	-1.599	-159+01	• 186-01						
-1.4	• 201	-1.346	-2.746	-1.196	-159+01	• 451-01						
-1.0	• 199	-0.950	-1.950	-0.801	-159+01	• 112+00						
-0.8	• 194	-0.755	-1.555	-0.601	-156+01	• 176+00						
-0.6	• 134	-0.563	-1.159	-0.416	-153+01	• 270+00						
-0.4	• 161	-0.402	-0.802	-0.236	-145+01	• 396+00						
-0.2	• 111	-0.273	-0.473	-0.086	-126+01	• 633+00						
0.0	• 025	-0.204	-0.204	-0.025	-106+01	-625+00						
0.2	• 095	-0.195	-0.001	• 005	-804+00	-632+00						
0.4	• 235	-0.235	-0.155	-0.165	-592+00	-592+00						
0.6	-400	-0.293	-0.307	-0.200	-398+00	-509+00						
0.8	-609	-0.375	-0.425	-0.191	-246+00	-421+00						
1.0	-876	-0.491	-0.509	-0.124	-113+00	-323+00						
1.2-1.199	-541	-0.559	-0.601	-0.632-01	-228+00							
1.4-1.562	-817	-0.593	-0.162	-0.274-01	-153+00							
1.6-1.345	-1.006	-0.594	-0.345	-0.113-01	-987-01							
1.8-2.339	-1.201	-0.599	-0.539	-0.459-02	-629-01							
2.0-2.736	-1.393	-0.601	-0.736	-0.134-02	-399-01							
2.2-2.135	-1.598	-0.602	-0.935	-0.733-03	-252-01							
2.4-3.534	-1.798	-0.602	-1.034	-0.292-03	-159-01							
2.6-7.934	-1.998	-0.602	-1.334	-0.116-03	-100-01							
2.8-4.334	-2.198	-0.602	-1.534	-0.464-04	-634-02							
3.0-4.734	-2.398	-0.602	-1.734	-0.185-04	-400-02							
3.1-5.534	-2.793	-0.602	-2.134	-0.292-05	-159-02							
3.6-6.334	-3.193	-0.602	-2.534	-0.464-06	-634-03							
4.2-7.134	-3.598	-0.602	-2.934	-0.735-07	-252-03							
4.6-7.934	-3.998	-0.602	-3.334	-0.116-07	-100-03							
5.0-8.734	-4.396	-0.602	-3.734	-0.400-08	-634-04							

EXACT ZINN EIGENVALUES

L1	LN	1/(LN)
1/1(LP)	1/1(LP)	1/1(LP)
-369+00	-284+01	-352+00
• 437+01	• 437+00	• 437+00

REDUCED DYNAMIC VISCOSITY AND VOLUMES

LOG	LOG	LOG	SUM	RECIP	SUM	SUM	H=• 130
OMT1	ETA1R	ETA2R	G1R	G2R	ETA1R	G1R	ETA1R
-2.8	-208	-2-742	-5-542	-2-592	-161+01	-181-02	-287-05
-2.0	-208	-1-642	-3-942	-1-792	-161+01	-114+01	-256-02
-1.8	-208	-1-742	-3-542	-1-592	-161+01	-181-01	-161+01
-1.4	-207	-1-343	-2-743	-1-193	-161+01	-454-01	-287-03
-1.0	-205	-0-946	-1-946	-795	-160+01	-113+00	-181-02
-0.8	-201	-752	-1-552	-599	-159+01	-177+00	-281-01
-0.6	-191	-566	-1-156	-409	-155+01	-272+00	-282+00
-0.4	-167	-368	-798	-233	-147+01	-400+00	-159+00
-0.2	-119	-263	-469	-061	-131+01	-529+00	-340+00
0	-033	-193	-199	-033	-108+01	-613+00	-633+00
2	-086	-191	-079	-114	-820+00	-644+00	-102+01
4	-227	-225	-175	-173	-593+00	-595+00	-150+01
6	-395	-282	-318	-205	-402+00	-529+00	-208+01
8	-610	-366	-434	-190	-245+00	-430+00	-272+01
1.0	-884	-485	-515	-115	-131+00	-327+00	-327+01
1.2-1.212	-638	-542	-512	-514-01	-230+00	-365+01	-973+00
1.4-1.578	-815	-585	-178	-264-01	-153+00	-385+01	-664+00
1.6-1.963	-1-005	-595	-363	-109-01	-989-01	-394+01	-434+00
1.8-2-357	-1-201	-599	-557	-440-02	-610-01	-397+01	-279+00
2.0-2-754	-1-399	-601	-754	-176-02	-399-01	-399+01	-176+00
2-2-3-153	-1-593	-602	-953	-703-03	-252-01	-400+01	-252-01
2-4-3-553	-1-798	-602	-1-153	-280-03	-159-01	-400+01	-704-01
2-6-3-953	-1-998	-602	-1-353	-112-03	-100-01	-400+01	-444-01
2-8-4-352	-2-193	-602	-1-552	-444-04	-634-03	-400+01	-280-02
3-0-4-752	-2-398	-602	-1-752	-177-04	-400-02	-400+01	-230-01
3-4-5-552	-2-798	-602	-2-152	-280-05	-159-02	-400+01	-704-02
3-8-6-352	-3-193	-602	-2-552	-444-06	-634-03	-400+01	-280-02
4-2-7-152	-3-598	-602	-2-952	-704-07	-252-03	-400+01	-112-02
4-6-7-952	-3-998	-602	-3-352	-112-07	-100-03	-400+01	-444-03
5-0-8-752	-4-398	-602	-3-752	-177-08	-400-04	-400+01	-177-03

EXACT LMM EIGENVALUES
 $L_1 \quad \ln \quad 1/(LN)$
 $3.367400 \cdot 2^{2401} \cdot 3^{367400}$

ב-99 רשות הדפסה ופומביות

EXACT ZIMM EIGENVALUES
 $L_1 \quad L_N \quad 1/(LN)$
 $362.00 \cdot 242.01 \cdot 413.00$

EXACT ZIMM EIGENVALUES
 $L_1 \quad L_N \quad I/(LN)$ SUM
 $1/(LP) \quad 1/(LP)$ RECIP
 $R_{OCAL} \quad (1/LP)^2 / LP^2$ SUM(L1 JER PHI
 $0.463+01 \quad 0.413+00 \quad 0.463+01 \quad 0.417 \quad 2.240$
 $0.362+00 \quad 0.242+01 \quad 0.413+00 \quad 0.417 \quad 2.240$

SYNTHETIC VISCOSITY AND MOSES

LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG
0MTI	ETA1R	ETA2R	G1R	G2R	ETA1R	ETA2R	0MTI	ETA1R
-2.8	-2.224	-2.732	-5.532	-2.576	-168+01	-195-02	-2.0	-1.932
-2.0	-2.224	-1.932	-3.932	-1.776	-158+01	-117-01	-2.0	-1.732
-1.8	-2.224	-1.732	-3.532	-1.576	-163+01	-195-01	-1.8	-1.332
-1.4	-2.224	-1.332	-2.732	-1.176	-157+01	-455-01	-1.4	-1.132
-1.0	-2.221	-0.936	-1.936	-0.773	-156+01	-116+00	-1.0	-0.936
-0.8	-2.17	-0.741	-1.541	-0.583	-155+01	-191+00	-0.8	-0.541
-0.6	-2.08	-0.555	-1.155	-0.392	-161+01	-279+00	-0.6	-0.155
-0.4	-1.85	-0.387	-0.787	-0.215	-153+01	-410+00	-0.4	-0.387
-0.2	-1.38	-0.256	-0.456	-0.062	-137+01	-555+00	-0.2	-0.256
0	-0.054	-0.182	-0.182	-0.054	-113+01	-557+00	0	-0.054
2	-0.064	-0.170	-0.030	-0.136	-664+00	-676+00	2	-0.064
4	-0.207	-0.195	-0.201	-0.193	-621+00	-632+00	4	-0.207
6	-0.395	-0.255	-0.345	-0.215	-412+00	-556+00	6	-0.395
8	-0.615	-0.343	-0.457	-0.185	-263+00	-454+00	8	-0.615
0	-0.305	-0.470	-0.530	-0.095	-124+00	-339+00	0	-0.305
2	-2.1247	-0.630	-0.570	-0.047	-557-01	-234+00	2	-2.1247
4	-1.4-1.620	-0.811	-0.589	-0.220	-240-01	-154+00	4	-1.4-1.620
6	-1.6-2.308	-1.003	-0.597	-0.408	-992-02	-992-01	6	-1.6-2.308
8	-1.8-2.403	-1.200	-0.600	-0.603	-395-02	-631-01	8	-1.8-2.403
0	-2.0-2.801	-1.399	-0.601	-0.801	-158-02	-399-01	0	-2.0-2.801
2	-2.2-3.201	-1.598	-0.602	-1.001	-630-03	-252-01	2	-2.2-3.201
4	-2.4-3.600	-1.798	-0.602	-1.200	-251-03	-159-01	4	-2.4-3.600
6	-2.6-4.000	-1.993	-0.602	-1.400	-100-03	-100-01	6	-2.6-4.000
8	-2.8-4.400	-2.198	-0.602	-1.600	-398-04	-634-03	8	-2.8-4.400
0	-3.0-4.800	-2.398	-0.602	-1.800	-158-04	-400-02	0	-3.0-4.800
2	-3.4-5.600	-2.798	-0.602	-2.000	-251-05	-159-02	2	-3.4-5.600
4	-3.8-6.400	-3.196	-0.602	-2.600	-398-06	-634-03	4	-3.8-6.400
6	-4.2-7.200	-3.598	-0.602	-3.000	-631-07	-252-03	6	-4.2-7.200
8	-4.6-8.000	-3.998	-0.602	-3.400	-100-07	-100-03	8	-4.6-8.000
0	-5.0-8.800	-4.398	-0.602	-3.800	-158-08	-400-04	0	-5.0-8.800

• 357 • 00 • 213 • 01 • 471 • 00
EXACT ZIMM EIGENWALDES
L1 LN 1/161

SUM	RECIP	SUM	SUM(L1)	H=4	H=250	PHI
L1/LP	ROCAL	(1/LP) ²	/LP) ²	-23	-23	
1.731	.578	.939+01	1.1959	.399	2.935	

REFUGEE CYRAN JOURNAL UND MÜNZEN

2 99 3 99 1 0.1951 1 0.1951 2

EXACT ZINN EIGENVALUES

L1	LN	LN(LN)	SUM	RECIP	SUM	SUM(LP)	JFR	H = .075
-129+00	-339+01	-295+00	-131+02	1.690	.592	(1/LP)2	1.1129	-360 .840
-23								

REDUCED DYNAMIC VISCOSITY AND MODULUS

CHI	FTAIR	FTA2R	G12	G18	FTA2R	G1R	G2R	MON	ARCTAN
-2.8	-2.228	-2.754	-5.554	-2.572	-1.59+01	-176-02	-280-05	-268-02	-169+01
-2.0	-2.228	-1.954	-3.954	-1.772	-1.69+01	-111-01	-111-03	-169-01	-169+01
-1.8	-2.228	-1.754	-3.554	-1.572	-1.69+01	-175-01	-279-03	-268-01	-658+02
-1.4	-2.228	-1.354	-2.754	-1.172	-1.69+01	-442-01	-176-02	-169+01	-104-01
-1.0	-2.225	-0.557	-1.957	-0.775	-0.555	-140+01	-521+00	-329+00	-164+01
-0.6	-2.212	-0.578	-1.178	-0.388	-0.163+01	-265+00	-499+01	-664+01	-357+00
-0.2	-0.367	-0.216	-0.16	-0.067	-0.067	-1.7+01	-507+00	-665+01	-494+01
0	-0.3	-0.036	-0.016	-0.007	-0.007	-0.5+00	-431+00	-272+01	-222+01
0.4	-0.212	-0.190	-0.111	-0.016	-0.016	-0.1+00	-434+00	-272+01	-182+01
0.6	-0.221	-0.145	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-126+01
0.8	-0.222	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-111+00
1.0	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-800-04
1.2	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
1.4	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
1.6	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
1.8	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
2.0	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
2.2	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
2.4	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
2.6	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
2.8	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
3.0	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
3.2	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
3.4	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
3.6	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
3.8	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
4.0	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
4.2	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
4.4	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
4.6	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
4.8	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01
5.0	-0.223	-0.146	-0.083	-0.005	-0.005	-0.5+00	-437+00	-272+01	-157+01

EXACT ZIMM EIGENVALUES
 $\lambda_1 = \lambda_N = 1/16\pi$
 $\bullet 132+0 \bullet 322+01 \bullet 310+00$

N = 8	H = 10
SUM	SUM(L1)
(1/LP)2	/LP)2
644.02	1.1205
	* 379
	1.116
	-23
	PHI

REDUCED CYANAMIC VISCOSITY AND MOULDRUNS

EXACT ZIMM EIGENWÄLDES
ל ז מ א נ וְ ז י מ א צ א כ א ת

CYANAMIC VISCOSITY AND MUDROUS AGEDEUCED

ARCTAN		MOD									
LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	ETAR
OMTI	ETAIR	ETA2R	61R	62R	ETAIR	ETA2R	G1R	62R	G1R	ETAR	ETA2/1
-2.8	-2.45	-2.747	-5.547	-2.555	-176+01	-179-02	-284-05	-279-02	-176+01	-102-02	-102-02
-2.0	-2.45	-1.947	-3.947	-1.755	-176+01	-113-01	-113-03	-176-01	-176+01	-643-02	-643-02
-1.8	-2.45	-1.747	-3.547	-1.555	-176+01	-179-01	-284-03	-279-01	-176+01	-102-01	-102-01
-1.4	-2.45	-1.347	-2.747	-1.155	-176+01	-449-01	-179-02	-700-01	-176+01	-256-01	-256-01
-1.0	-2.43	-0.951	-1.951	-0.757	-175+01	-112-01	-112-01	-175+01	-175+01	-640-01	-640-01
-0.8	-2.39	-0.756	-1.556	-0.561	-173+01	-175+00	-278-01	-275+00	-174+01	-101+00	-101+00
-0.6	-2.30	-0.570	-1.170	-0.370	-170+01	-263+00	-675-01	-426+00	-172+01	-157+00	-157+00
-0.4	-2.09	-0.403	-0.803	-0.191	-162+01	-395+00	-157+00	-644+00	-166+01	-240+00	-240+00
-0.2	-1.65	-0.274	-0.474	-0.035	-146+01	-512+00	-335+00	-923+00	-156+01	-349+00	-349+00
0	-0.090	-0.206	-0.206	-0.090	-123+01	-623+00	-623+00	-123+01	-138+01	-469+00	-469+00
0.2	-0.009	-0.200	-0.200	-0.000	-191	-979+00	-631+00	-100+01	-155+01	-117+01	-572+00
0.4	-0.117	-0.232	-0.232	-0.168	-283	-764+00	-586+00	-147+01	-192+01	-963+00	-654+00
0.6	-0.232	-0.279	-0.321	-0.368	-586+00	-526+00	-209+01	-233+01	-79+00	-731+00	-731+00
0.8	-0.362	-0.334	-0.456	-0.438	-434+00	-453+00	-292+01	-274+01	-635+00	-818+00	-818+00
1.0	-0.519	-0.400	-0.600	-0.481	-363+00	-398+00	-398+01	-303+01	-500+00	-921+00	-921+00
1.2	-0.718	-0.484	-0.716	-0.492	-191+00	-328+00	-520+01	-303+01	-380+00	-104+01	-104+01
1.4	-0.975	-0.598	-0.902	-0.425	-106+00	-253+00	-635+01	-266+01	-274+00	-117+01	-117+01
1.6	-1.290	-0.745	-0.855	-0.310	-513-01	-180+00	-717+01	-204+01	-187+00	-129+01	-129+01
1.8	-1.647	-0.918	-0.832	-0.153	-225-01	-121+00	-763+01	-142+01	-123+00	-139+01	-139+01
2.0	-2.028	-1.105	-0.895	-0.028	-937-02	-794+01	-784+01	-937+00	-79+01	-115+01	-115+01
2.2	-2.421	-1.300	-0.900	-0.221	-380-02	-501-01	-794+01	-602+00	-502-01	-150+01	-150+01
2.4	-2.817	-1.498	-0.902	-0.417	-152-02	-317-01	-797+01	-782+00	-318-01	-152+01	-152+01
2.6	-3.216	-1.597	-0.903	-0.615	-608-03	-201-01	-799+01	-242+00	-201-01	-154+01	-154+01
2.8	-3.616	-1.897	-0.903	-0.816	-242-03	-127-01	-800+01	-153+00	-127-01	-155+01	-155+01
3.0	-4.015	-2.057	-0.903	-1.015	-965-04	-800-02	-800+01	-965-01	-800-02	-156+01	-156+01
3.4	-4.815	-2.497	-0.903	-1.415	-153-04	-318-02	-800+01	-384-01	-318-02	-157+01	-157+01
3.8	-5.615	-2.897	-0.903	-1.815	-242-05	-127-02	-800+01	-153-01	-127-02	-157+01	-157+01
4.2	-6.415	-3.297	-0.903	-2.215	-384-06	-505-03	-800+01	-609-02	-505-03	-157+01	-157+01
4.6	-7.215	-3.697	-0.903	-2.615	-609-07	-201-03	-800+01	-242-02	-201-03	-157+01	-157+01
5.0	-8.015	-4.097	-0.903	-3.015	-965-08	-800-04	-800+01	-965-03	-800-04	-157+01	-157+01

EXACT ZIMM EIGENVALUES
L1 LN 1/11N1
37+81 45+80 290+81 0+81

N = 9	H = 150
SUM	SUM(L1)
(1/LP)2	LP/2
• 602 • 02	1 • 1375
	• 357
	1 • 6668
	- 23

סְדֻכֶּה כַּיָּמִים וְעַתָּה וְעַתָּה מִנְדָּרָעָם

卷之三

• 143-00 257-01 • 390-00
EXACT SIZE ENGRAVED
LI LN 1/16IN

	RECIP	SUM	N = 8	H = .20
L1/LP	ROCAL	SUM(L1/LP)2	• 567 • 02	1.1572
L1/LP	RECIP	SUM(L1/LP)2	• 02	• 334
L1/LP	ROCAL	SUM(L1/LP)2	• 00	2.228

REDUCED DYNAMIC VISCOSITY AND MOLENTUS

EXACT ZIMM EIGENVALUES

EXACT ZINN EIGENVALUES
 $\lambda_1 = 148.00$ $\lambda_2 = 224.01$
 $\lambda_3 = 447.00$ $\lambda_4 = 447.00$
 $\lambda_5 = 946.00$ $\lambda_6 = 946.00$
 $\lambda_7 = 131.02$ $\lambda_8 = 131.02$
 $\lambda_9 = 514.00$ $\lambda_{10} = 514.00$
 $\lambda_{11} = 538.02$ $\lambda_{12} = 538.02$
 $\lambda_{13} = 1180.7$ $\lambda_{14} = 1180.7$
 $\lambda_{15} = 312.00$ $\lambda_{16} = 312.00$
 $\lambda_{17} = 2810.00$ $\lambda_{18} = 2810.00$

REDUCED SYNTHETIC VISCOSITY AND MOULDS

ARCTIC									
MON	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP
LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG
OMTI	FTAIR	ETA2R	G10	G2R	ETAIR	G1R	ETA2R	G2R	ETAR
-2.8	+289	-2.728	-5.528	-2.511	+195+71	+187-02	+297-05	+309-02	+195+31
-2.0	+299	-1.928	-3.928	-1.711	+195+01	+118-01	+117-03	+195-01	+195+01
-1.8	+289	-1.728	-3.528	-1.511	+165+01	+187-01	+297-01	+308-01	+195+01
-1.4	+289	-1.328	-2.728	-1.111	+164+01	+469-01	+187-02	+774-01	+195+01
-1.0	+287	-0.932	-1.932	-0.713	+194+01	+117+00	+117+01	+241-01	+195+01
-0.8	+233	-0.737	-1.537	-0.517	+192+01	+183+00	+290-01	+304+00	+194+01
-0.6	+275	-0.551	-1.151	-0.325	+188+01	+291+00	+707-01	+473+00	+194+00
-0.4	+266	-0.382	-0.782	-0.144	+180+01	+415+00	+165+00	+718+00	+185+01
-0.2	+216	-0.250	-0.450	+0.16	+184+01	+562+00	+355+00	+104+01	+174+01
0	+148	-0.175	-0.175	+148	+140+1	+666+00	+666+00	+140+01	+156+01
2	+0.56	-0.157	-0.043	+256	+114+01	+996+00	+110+01	+180+01	+133+01
4	-0.048	-0.175	-0.225	+352	+896+00	+658+00	+168+01	+225+01	+112+01
6	-0.165	-0.208	-0.435	+392	+687+00	+620+00	+247+01	+272+01	+737+00
8	-0.309	-0.254	-0.546	+491	+491+00	+558+00	+352+01	+310+01	+743+00
0	-0.494	-0.320	-0.680	+506	+321+00	+479+00	+479+01	+321+01	+576+00
1.2	-0.737	-0.419	+781	+463	+183+00	+381+00	+604+01	+293+00	+423+01
1.4	-0.175	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
2.0	-0.056	-0.043	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
2.2	-0.48	-0.175	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
2.6	-0.165	-0.208	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
3.0	-0.0	-0.157	+0.43	+546	+321+00	+479+00	+479+01	+321+01	+576+00
3.2	-0.2	-0.043	+680	+506	+183+00	+381+00	+604+01	+293+00	+423+01
3.4	-0.4	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
3.6	-0.6	-0.225	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
3.8	-0.1	-0.043	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
4.0	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
4.2	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
4.4	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
4.6	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
4.8	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
5.0	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
5.2	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
5.4	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
5.6	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
5.8	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
6.0	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
6.2	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
6.4	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
6.6	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
6.8	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
7.0	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
7.2	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
7.4	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
7.6	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
7.8	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
8.0	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
8.2	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
8.4	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
8.6	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
8.8	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
9.0	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
9.2	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
9.4	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
9.6	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
9.8	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
10.0	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
10.2	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
10.4	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
10.6	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
10.8	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
11.0	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
11.2	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
11.4	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
11.6	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
11.8	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
12.0	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
12.2	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
12.4	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
12.6	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
12.8	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
13.0	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
13.2	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
13.4	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
13.6	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
13.8	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
14.0	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
14.2	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
14.4	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
14.6	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
14.8	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
15.0	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
15.2	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
15.4	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
15.6	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
15.8	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
16.0	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
16.2	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
16.4	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
16.6	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
16.8	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
17.0	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
17.2	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
17.4	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
17.6	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
17.8	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
18.0	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
18.2	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
18.4	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
18.6	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
18.8	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
19.0	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
19.2	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
19.4	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
19.6	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
19.8	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
20.0	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
20.2	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
20.4	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
20.6	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
20.8	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
21.0	-0.2	-0.056	+256	+114+01	+996+00	+110+01	+194+00	+277+00	+136+01
21.2	-0.6	-0.165	+352	+392	+687+00	+620+00	+247+01	+272+01	+737+00
21.4	-0.4	-0.0	+435	+491	+491+00	+558+00	+352+01	+310+01	+743+00
21.6	-0.8	-0.175	+148	+140+1	+666+00	+666+00	+129+01	+228+01	+129+00
21.8									

• 149•pg • 216•01 • 463•00

EXACT ZIMM EIGENVALUES		N = 9		N = 12	
L1	LN	SUM	RECIP	SUM	RECIP
1.149+00	216+01	4.63+00	1.32+02	1.162	1.162
1.149-00	216-01	4.63-00	1.32-02	1.160	1.160
-1.149+00	216+01	4.63+00	1.32+02	1.162	1.162
-1.149-00	216-01	4.63-00	1.32-02	1.160	1.160

MISSISSIPPI EXAMINER AND ADVERTISING COMPANY.

#1250

EXACT ZIMM EIGENVALUES
 L₁ L_N I / (L_N)
 1.93-01 • 347+01 • 288+00

EXACT ZIMM EIGENVALUES					
L_1	\ln	$1/(LN)$	SUM	RECIP	SUM
•1.93-01	•347+01	•288+00	•927+02	1.791	1/LP
				•5558	(1/LP)2
				•297+04	(1/LP)1
				1.1097	SUM(L1)
				•346	JER
				1.077	PHI
				-23	

REDUCED CYANAMIC VISCOSITY AND MODULUS

EXACT ZMM EIGENVALUES

L1	LN	1/1N1	1/(LP1)	1/(LP1)	SUM	RECIP	SUM	SUM	RECIP	SUM	SUM	RECIP	1/(LP1)2	1/(LP1)2	-23
•209-01	•330+01	•303+00	•881+02	1+840	•543	•256+04	1+1177	•330	1+364						

PREDUCED DYNAMIC VISCOSITY AND MODULUS

LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG
0M11 FTAIR ETAF2R	G12	628	ETAF18	ETAF2R	G12	628	ETAF18	ETAF2R	G12	628	ETAF18	ETAF2R	G12	628	ETAF18	ETAF2R
-2.8	•265	-2.752	-5.552	-2.535	•184+01	•177-02	•281-05	•292-02	•194+01	•194+01	•963-03					
-2.0	•265	-1.952	-2.952	-1.735	•184+01	•12-01	•112-03	•184-01	•184+01	•184+01	•607-02					
-1.8	•265	-1.752	-3.552	-1.535	•184+01	•177-01	•281-03	•292-01	•184+01	•184+01	•963-02					
-1.4	•264	-1.352	-2.752	-1.136	•184+01	•444-01	•177-02	•732-01	•184+01	•184+01	•242-01					
-1.0	•262	-0.956	-1.956	-0.738	•183+01	•183+01	•111+00	•183+00	•183+01	•183+01	•605-01					
-0.8	•259	-0.761	-1.561	-0.541	•181+01	•173+00	•275-01	•288+00	•182+01	•182+01	•952-01					
-0.6	•250	-0.576	-1.176	-0.350	•178+01	•266+00	•667-01	•447+00	•180+01	•148+00						
-0.4	•230	-0.409	-0.809	-0.170	-0.170+01	•390+00	•155+00	•676+00	•174+01	•226+00						
-0.2	•189	-0.281	-0.481	-0.011	-0.154+01	•524+00	•330+00	•975+00	•163+01	•327+00						
0	•119	-0.214	-0.214	•119	•1+01	•611+00	•611+00	•131+01	•145+01	•435+00						
2	•028	-0.212	-0.012	•228	•107+01	•614+00	•552+00	•141+01	•215+01	•103+01	•580+00					
4	•067	-0.250	•150	•333	•858+00	•552+00	•316+00	•501+01	•546+01	•458+00	•743+00					
6	•161	-0.303	•297	•439	•590+00	•497+00	•198+00	•675+01	•658+01	•378+00	•791+00					
8	•258	-0.384	•436	•542	•552+00	•332+00	•273+01	•349+01	•701+00	•654+00						
10	•358	-0.431	•569	•642	•439+00	•371+00	•371+01	•439+01	•575+00	•702+00						
12	-463	-0.500	•700	•737	•345+00	•345+00	•316+00	•501+01	•546+01	•458+00						
14	-575	-0.571	•829	•825	•266+00	•266+00	•269+00	•675+01	•658+01	•378+00						
16	-701	-0.643	•957	•899	•199+00	•228+00	•906+01	•792+01	•915+01	•124+01						
18	-849	-0.719	1.031	•951	-141+00	•161+00	•121+02	•893+01	•218+00	•934+00						
20	-1.035	-0.806	1.194	•965	-922+01	•156+00	•501+01	•546+01	•458+00	•743+00						
24	-575	-0.916	1.284	•924	-529+01	•121+00	•192+02	•839+01	•132+00	•116+01						
26	-1.927	-1.227	1.373	•573	•118+01	•593+01	•236+02	•471+01	•605+01	•137+01						
28	-2.304	-1.412	1.398	•495	•497+02	•347+01	•244+02	•314+01	•390+01	•144+01						
30	-2.398	-1.412	1.398	•487	•818+05	•158+02	•250+02	•130+00	•130+00	•157+01						
32	-3.488	-2.003	1.367	•078	-0.88	-325-03	-994-02	-250+02	-816+00	-664-02	-154+01					
34	-4.087	-2.802	1.398	•887	-0.887	-818+05	•158+02	•250+02	•326+00	•396-02	•156+01					
36	-5.687	-3.202	1.398	•1.287	-1.287	-1.287	-1.287	-1.287	-1.287	-1.287	•157+01					
38	-6.687	-3.602	1.398	-1.687	-206-06	-206-06	-206-06	-206-06	-206-06	-206-06	•157+01					
40	-2.5087	-2.802	1.398	-1.687	-2.003	-2.003	-2.003	-2.003	-2.003	-2.003	•250+02					
42	-5.087	-2.802	1.398	-1.687	-3.488	-3.488	-3.488	-3.488	-3.488	-3.488	•250+02					
44	-2.5-0.087	-2.802	1.398	-1.687	-3.8-4.087	-2.8-4.087	-2.8-4.087	-2.8-4.087	-2.8-4.087	-2.8-4.087	•250+02					
46	-6.5-0.687	-3.202	1.398	-1.687	-3.1-3.488	-3.1-3.488	-3.1-3.488	-3.1-3.488	-3.1-3.488	-3.1-3.488	•250+02					
48	-6.687	-3.602	1.398	-1.687	-4.6-5.687	-4.6-5.687	-4.6-5.687	-4.6-5.687	-4.6-5.687	-4.6-5.687	•250+02					

EXACT ZIMM EIGENVALUES
 L_1 $\ln 1/(CLN)$ SUM $L_1/(LP)$ RECIP L_1/LP ROCAL $(1/LP)^2$ JFR
 $\cdot 228-n_1 \cdot 310+0_1 \cdot 323+0_0 \cdot 835+0_2 1.899 \cdot 527 \cdot 218+0_4 1.1270 \cdot 313 \cdot 1.681$

REDUCED DYNAMIC VISCOSITY AND MODULUS						MOD ARCTAN					
LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG
OMT1	ETAIR	ETAIR	G1R	G2R	ETAIR	ETAIR	G1R	G2R	ETAIR	ETAIR	ETAIR
-2.8	-27.8	-2.748	-5.548	-2.522	-160+0_1	-179-0_2	-283-0_5	-301-0_2	-180+0_1	-941-0_3	
-2.0	-27.8	-1.948	-3.948	-1.722	-190+0_1	-113-0_1	-113-0_3	-190+0_1	-190+0_1	-594-C2	
-1.8	-27.8	-1.748	-3.548	-1.522	-190+0_1	-179-0_1	-283-0_3	-301-0_1	-190+0_1	-941-G2	
-1.4	-27.8	-1.349	-2.749	-1.122	-190+0_1	-448-0_1	-178-0_2	-755-0_1	-190+0_1	-236-0_1	
-1.0	-27.6	-0.952	-1.952	-0.724	-189+0_1	-112+0_0	-112+0_1	-189+0_0	-189+0_1	-591-0_1	
-0.8	-27.3	-0.758	-1.558	-0.527	-187+0_1	-175+0_0	-277+0_1	-297+0_0	-188+0_1	-930-0_1	
-0.6	-26.4	-0.572	-1.172	-0.336	-184+0_1	-268+0_0	-673-0_1	-462+0_0	-186+0_1	-145+0_0	
-0.4	-24.5	-0.405	-0.805	-0.155	-176+0_1	-394+0_0	-157+0_0	-700+0_1	-180+0_1	-220+0_0	
-0.2	-20.5	-0.276	-0.476	-0.005	-150+0_1	-529+0_0	-334+0_0	-101+0_1	-169+0_1	-319+0_0	
0	-13.7	-0.208	-0.208	-0.137	-137+0_1	-620+0_0	-620+0_0	-137+0_1	-150+0_1	-424+0_0	
2	-0.49	-0.204	-0.004	-0.249	-112+0_1	-626+0_0	-992+0_0	-178+0_1	-128+0_1	-510+0_0	
4	-0.43	-0.238	-0.162	-0.357	-906+0_0	-578+0_0	-145+0_1	-228+0_1	-107+0_1	-567+0_0	
6	-1.35	-0.288	-0.312	-0.465	-733+0_0	-515+0_0	-205+0_1	-292+0_1	-896+0_0	-612+0_0	
8	-2.30	-0.346	-0.454	-0.570	-589+0_0	-451+0_0	-285+0_1	-372+0_1	-742+0_0	-653+0_0	
10	-3.29	-0.408	-0.592	-0.671	-469+0_0	-391+0_0	-391+0_1	-469+0_1	-610+0_0	-694+0_0	
12	-4.34	-0.474	-0.726	-0.766	-368+0_0	-336+0_0	-532+0_1	-584+0_1	-498+0_0	-739+0_0	
14	-5.48	-0.541	-0.859	-0.852	-283+0_0	-288+0_0	-723+0_1	-711+0_1	-404+0_0	-794+0_0	
16	-6.78	-0.610	-0.990	-0.922	-210+0_0	-245+0_0	-677+0_1	-815+0_1	-323+0_0	-864+0_0	
18	-8.36	-0.686	-1.114	-0.964	-146+0_0	-206+0_0	-130+0_2	-921+0_1	-253+0_0	-955+0_0	
20	-1.037	-0.777	-1.223	-0.963	-918-0_1	-157+0_0	-167+0_2	-246+0_1	-392+0_1	-146+0_1	
22	-1.298	-0.895	-1.305	-0.902	-504+0_1	-127+0_0	-202+0_2	-799+0_1	-137+0_0	-119+0_1	
24	-1.619	-1.046	-1.354	-0.784	-242+0_1	-900-0_1	-226+0_2	-608+0_1	-932+0_1	-121+0_1	
26	-1.976	-1.221	-1.379	-0.624	-105-0_1	-601-0_1	-239+0_2	-421+0_1	-610+0_1	-107+0_1	
28	-2.359	-1.410	-1.390	-0.441	-438-0_2	-389-0_1	-248-0_1	-177+0_1	-249+0_1	-54+0_1	
30	-2.751	-1.605	-1.395	-0.249	-177-0_2	-248-0_1	-248+0_2	-177+0_1	-249+0_1	-54+0_1	
32	-3.547	-2.003	-1.397	-0.147	-284-0_3	-994-0_2	-250+0_2	-713+0_0	-995-0_2	-54+0_1	
34	-4.346	-2.402	-1.398	-0.546	-450-0_4	-396-0_2	-250+0_2	-284+0_0	-396-0_2	-156+0_1	
36	-5.146	-2.802	-1.308	-0.946	-714-0_5	-158-0_2	-250+0_2	-113+0_0	-158-0_2	-157+0_1	
38	-5.946	-3.202	-1.398	-1.346	-113-0_5	-628-0_3	-250+0_2	-451-0_1	-628-0_3	-157+0_1	
40	-6.746	-3.602	-1.398	-1.746	-179-0_6	-250-0_3	-250+0_2	-179-0_1	-250-0_3	-157+0_1	

EXACT ZIMM EIGENVALUES
 L_1 \ln $1/(LN)$ SUM RECIP SUM $(1/LP)_1$ $(1/LP)_2$ JER PHI
•240-01 • 296+01 • 337+00 • 808+02 1.938 • 516 • 197+04 1.1331 • 302 1.877

REDUCED DYNAMIC VISCOSITY AND MODULUS									
LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG
0.071	ETA1R	ETA2R	G1R	G2R	ETA1R	ETA2R	G1R	G2R	ETA1R
-2.8	• 287	-2.746	-5.546	-2.513	• 194+01	• 180-02	• 285-05	• 307-02	• 194+01
-2.0	• 287	-1.946	-3.946	-1.712	• 194+01	• 113-01	• 113-03	• 194-01	• 194+01
-1.8	• 287	-1.746	-3.546	-1.513	• 194+01	• 180-01	• 285-03	• 307-01	• 194+01
-3.4	• 287	-1.346	-2.746	-1.113	• 194+01	• 450-01	• 179-02	• 771-01	• 194+01
-1.0	• 285	-0.950	-1.950	-0.715	1.92+01	• 112+00	• 112-01	• 193+00	• 192+01
-0.8	• 282	-0.755	-1.555	-0.513	1.91+01	• 176+00	• 278-01	• 303+00	• 192+01
-0.6	• 273	-0.569	-1.169	-0.327	1.88+01	• 270+00	• 677-01	• 471+00	• 190+01
-0.4	• 254	-0.402	-0.802	-0.146	1.80+01	• 396+00	• 158+00	• 715+00	• 184+01
-0.2	• 215	-0.273	-0.473	• 0.115	1.54+01	• 513+00	• 336+00	• 104+01	• 173+01
0.0	• 149	-0.204	-0.204	• 1.49	1.41+01	• 625+00	• 625+00	• 141+01	• 154+01
0.2	• 063	-0.198	-0.062	-0.263	• 116+01	• 634+00	• 100+01	• 183+01	• 132+01
0.4	-0.027	-0.231	• 169	• 373	• 940+00	• 568+00	• 148+01	• 236+01	• 111+01
0.6	-1.18	-0.278	• 322	• 482	• 762+00	• 527+00	• 210+01	• 303+01	• 927+00
0.8	-2.12	-0.334	• 456	• 588	• 514+00	• 454+00	• 293+01	• 388+01	• 778+00
1.0	-3.10	-0.394	• 606	• 690	• 490+00	• 404+00	• 404+01	• 490+01	• 635+00
1.2	-4.15	-0.456	• 744	• 785	• 394+00	• 350+00	• 554+01	• 609+01	• 527+00
1.4	-5.31	-0.521	• 879	• 869	• 295+00	• 301+00	• 757+01	• 740+01	• 421+00
1.6	-6.65	-0.589	• 935	• 216+00	• 258+00	• 103+02	• 862+01	• 337+00	• 872+00
1.8	-8.29	-0.664	• 1.136	• 971	• 148+00	• 217+00	• 137+02	• 935+01	• 971+00
2.0	-1.041	-0.759	• 1.241	• 959	• 909-01	• 174+00	• 174+02	• 909+01	• 197+00
2.2	-2.1314	-0.883	• 1.317	• 986	• 485-01	• 131+00	• 207+02	• 769+01	• 140+00
2.4	-4.1643	-1.039	• 1.351	• 757	-227-01	-6.13-01	-226+01	• 571+01	• 941-01
2.6	-2.009	-1.218	• 1.382	• 591	• 979-02	• 505-01	• 241+02	• 390+01	• 613-01
2.8	-2.335	-1.459	• 1.391	• 475	• 403-02	• 390-01	• 246+02	• 254+01	• 392-01
3.0	-2.789	-1.605	• 1.393	• 211	• 163-02	• 248-01	• 248+02	• 163+01	• 249-01
3.2	-3.585	-2.002	• 1.398	• 185	• 260-01	• 994-02	• 250+02	• 653+00	• 995-02
3.4	-4.385	-2.402	• 1.398	• 585	• 12-04	• 396-02	• 250+02	• 260+00	• 396-02
4.0	-2.5185	-2.802	• 1.398	• 985	• 554-05	• 558-02	• 250+02	• 104+00	• 158-02
4.6	-5.985	-3.202	• 1.398	• 385	• 104-05	• 628-03	• 250+02	• 413-01	• 628-03
5.0	-6.785	-3.602	• 1.378	• 785	• 164-06	• 250-03	• 250+02	• 164-01	• 250-03
									• 157+01

EXACT ZIMM EIGENVALUES
L1 LN L1(LN)
.270-01 .262+01 .381+00

REDUCED DYNAMIC VISCOSITY AND MODULUS

EXACT ZIMM EIGENVALUES
L1 LN 1/1LN
308-01 -220+01 -454+00

EXACT ZIMM EIGENVALUES				N=25 H=0.262			
L1	LN	LN(LN)	SUM	RECIP	SUM	SUM(L1)	JFR PHI
1.308-01	220+01	-454+00	.706+02	2.173	.460	(1/LP)2	-23
						(1/LP)2	
						1.123+04	1.1659 .247 2.864

REFRACTIVE DYNAMIC VISCOSITY AND MOULDS

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EXACT ZINN EIGENVALUES
L1 L2 L3 L4 L5 L6 L7 L8 L9 L10

M	SUM	RECIP	SUM	SUM(LP)	JER	PHI
LP)	L/LP	ROCAL	(1/LP)2	(LP)2		
5+02	2.263	•442	•108+04	1.1773	•230	3.183
					-23	

РЕДУКЦИЯ CYANAMIC VISCOSITY AND **МОДУЛЬ УСИЛИЯ**

LOG	LOG	LOG	LOG	OMT1	ETA1R	ETA2R	G19	G29	ETA1R	FTA2R	G18	G2R	ETA1R	FTA2R	G19	G29	ETA1R	FTA2R	G18	G2R	ETA1R	FTA2R	G19	G29	LOG	LOG					
-2.8	• 355	-2.729	-5.529	-2.445	• 226+01	• 197-02	• 296-05	• 359-02	-226+01	• 226+01	• 359-02	• 226+01	• 197-02	• 296-05	• 359-02	• 226+01	• 197-02	• 296-05	• 359-02	• 226+01	• 197-02	• 296-05	• 359-02	• 226+01	• 197-02	• 296-05	• 359-02	-2.8	• 355		
-2.0	• 355	-1.929	-3.929	-1.643	• 226+01	• 197-01	• 296-04	• 359-01	-226+01	• 197-01	• 296-04	• 359-01	• 226+01	• 197-01	• 296-04	• 359-01	• 226+01	• 197-01	• 296-04	• 359-01	• 226+01	• 197-01	• 296-04	• 359-01	• 226+01	• 197-01	• 296-04	• 359-01	-2.0	• 355	
-1.6	• 355	-1.729	-3.529	-1.445	• 226+01	• 197-01	• 296-03	• 359-01	-226+01	• 197-01	• 296-03	• 359-01	• 226+01	• 197-01	• 296-03	• 359-01	• 226+01	• 197-01	• 296-03	• 359-01	• 226+01	• 197-01	• 296-03	• 359-01	• 226+01	• 197-01	• 296-03	• 359-01	-1.6	• 355	
-1.4	• 354	-1.330	-2.730	-1.045	• 226+01	• 196-01	• 186-07	• 900-01	-226+01	• 196-01	• 186-07	• 900-01	• 226+01	• 196-01	• 186-07	• 900-01	• 226+01	• 196-01	• 186-07	• 900-01	• 226+01	• 196-01	• 186-07	• 900-01	• 226+01	• 196-01	• 186-07	• 900-01	-1.4	• 354	
-1.0	• 353	-0.933	-1.933	-0.647	• 225+01	• 117-00	• 117-01	• 225+00	-225+00	• 117-01	• 225+00	• 225+00	-225+00	• 117-01	• 225+00	• 225+00	-225+00	• 117-01	• 225+00	• 225+00	-225+00	• 117-01	• 225+00	• 225+00	-225+00	• 117-01	• 225+00	• 225+00	-225+00	-1.0	• 353
-0.8	• 350	-0.738	-1.538	-0.450	• 224+01	• 183+00	• 289-01	• 355+00	-224+01	• 183+00	• 289-01	• 355+00	-224+01	• 183+00	• 289-01	• 355+00	-224+01	• 183+00	• 289-01	• 355+00	-224+01	• 183+00	• 289-01	• 355+00	-224+01	• 183+00	• 289-01	• 355+00	-0.8	• 350	
-0.6	• 343	-0.552	-1.152	-0.257	• 220+01	• 281+00	• 705-01	• 553+00	-220+01	• 281+00	• 705-01	• 553+00	-220+01	• 281+00	• 705-01	• 553+00	-220+01	• 281+00	• 705-01	• 553+00	-220+01	• 281+00	• 705-01	• 553+00	-220+01	• 281+00	• 705-01	• 553+00	-0.6	• 343	
-0.4	• 326	-0.384	-0.784	-0.074	• 212+01	• 413+00	• 165+00	• 844+00	-212+01	• 413+00	• 165+00	• 844+00	-212+01	• 413+00	• 165+00	• 844+00	-212+01	• 413+00	• 165+00	• 844+00	-212+01	• 413+00	• 165+00	• 844+00	-212+01	• 413+00	• 165+00	• 844+00	-0.4	• 326	
-0.2	• 263	-0.252	-0.452	• 0.93	• 196+01	• 560+00	• 353+00	• 124+01	-0.252	• 196+01	• 560+00	• 353+00	-0.252	• 196+01	• 560+00	• 353+00	-0.252	• 196+01	• 560+00	• 353+00	-0.252	• 196+01	• 560+00	• 353+00	-0.252	• 196+01	• 560+00	• 353+00	-0.2	• 263	
0.0	• 236	-0.177	-0.177	• 235	• 172+01	• 556+00	• 666+00	• 172+01	• 235	• 172+01	• 556+00	• 666+00	• 235	• 172+01	• 556+00	• 666+00	• 235	• 172+01	• 556+00	• 666+00	• 235	• 172+01	• 556+00	• 666+00	• 235	• 172+01	• 556+00	• 666+00	0.0	• 236	
0.2	• 164	-0.160	-0.040	• 364	• 146+01	• 549+00	• 104+01	• 443+00	-0.160	• 146+01	• 549+00	• 104+01	-0.160	• 146+01	• 549+00	• 104+01	-0.160	• 146+01	• 549+00	• 104+01	-0.160	• 146+01	• 549+00	• 104+01	-0.160	• 146+01	• 549+00	• 104+01	0.2	• 164	
0.4	• 087	-0.177	-0.177	• 223	• 487	• 192+01	• 655+00	• 167+01	• 362+01	-0.177	• 487	• 192+01	• 655+00	• 167+01	-0.177	• 487	• 192+01	• 655+00	• 167+01	-0.177	• 487	• 192+01	• 655+00	• 167+01	-0.177	• 487	• 192+01	• 655+00	• 167+01	0.4	• 087
0.6	• 008	-0.207	-0.207	• 293	• 608	• 102+01	• 622+00	• 247+01	• 405+01	-0.207	• 608	• 102+01	• 622+00	• 247+01	-0.207	• 608	• 102+01	• 622+00	• 247+01	-0.207	• 608	• 102+01	• 622+00	• 247+01	-0.207	• 608	• 102+01	• 622+00	• 247+01	0.6	• 008
0.8	-0.077	-0.241	-0.559	• 723	• 837+00	• 574+07	• 362+01	• 102+01	-0.077	• 723	• 837+00	• 574+07	• 362+01	-0.077	• 723	• 837+00	• 574+07	• 362+01	-0.077	• 723	• 837+00	• 574+07	• 362+01	-0.077	• 723	• 837+00	• 574+07	• 362+01	0.8	-0.077	
1.0	-0.171	-0.273	-0.722	• 820	• 674+00	• 527+00	• 527+01	• 574+01	-0.171	• 820	• 674+00	• 527+00	• 527+01	-0.171	• 820	• 674+00	• 527+00	• 527+01	-0.171	• 820	• 674+00	• 527+00	• 527+01	-0.171	• 820	• 674+00	• 527+00	• 527+01	1.0	-0.171	
1.2	-0.281	-0.318	-0.882	• 919	• 523+00	• 481+00	• 763+01	• 829+00	-0.281	• 919	• 523+00	• 481+00	• 763+01	• 829+00	-0.281	• 919	• 523+00	• 481+00	• 763+01	• 829+00	-0.281	• 919	• 523+00	• 481+00	• 763+01	• 829+00	-0.281	• 919			
1.4	-0.418	-0.364	-1.036	• 982	• 392+00	• 109+02	• 432+01	• 109+02	-0.418	• 982	• 392+00	• 109+02	• 432+01	• 109+02	-0.418	• 982	• 392+00	• 109+02	• 432+01	• 109+02	-0.418	• 982	• 392+00	• 109+02	• 432+01	• 109+02	-0.418	• 982			
1.6	-0.599	-0.429	-0.926	• 711	• 133+01	• 971+01	• 373+00	• 971+01	-0.599	• 711	• 133+01	• 971+01	• 373+00	• 971+01	-0.599	• 711	• 133+01	• 971+01	• 373+00	• 971+01	-0.599	• 711	• 133+01	• 971+01	• 373+00	• 971+01	-0.599	• 711			
1.8	-0.840	-0.650	-1.455	• 960	• 145+00	• 298+00	• 298+00	• 960	-0.840	• 960	• 145+00	• 298+00	• 298+00	-0.840	• 960	• 145+00	• 298+00	• 298+00	-0.840	• 960	• 145+00	• 298+00	• 298+00	-0.840	• 960	• 145+00	• 298+00	• 298+00	-0.840	• 960	
2.0	-0.490	-0.349	-0.542	• 101	• 542+00	• 244+02	• 244+02	• 542+01	-0.490	• 101	• 542+00	• 244+02	• 244+02	-0.490	• 101	• 542+00	• 244+02	• 244+02	-0.490	• 101	• 542+00	• 244+02	• 244+02	-0.490	• 101	• 542+00	• 244+02	• 244+02	-0.490	• 101	
2.2	-0.626	-0.216	-0.394	• 349	• 334	• 145+00	• 145+00	• 349	-0.626	• 349	• 334	• 145+00	• 145+00	-0.626	• 349	• 334	• 145+00	• 145+00	-0.626	• 349	• 334	• 145+00	• 145+00	-0.626	• 349	• 334	• 145+00	• 145+00	-0.626	• 349	
2.4	-0.786	-0.002	-1.398	• 103	• 387	• 145+00	• 145+00	• 103	-0.786	• 103	• 387	• 145+00	• 145+00	-0.786	• 103	• 387	• 145+00	• 145+00	-0.786	• 103	• 387	• 145+00	• 145+00	-0.786	• 103	• 387	• 145+00	• 145+00	-0.786	• 103	
2.6	-2.266	-1.216	-1.394	• 394	• 394	• 145+00	• 145+00	• 394	-2.266	• 394	• 394	• 145+00	• 145+00	-2.266	• 394	• 394	• 145+00	• 145+00	-2.266	• 394	• 394	• 145+00	• 145+00	-2.266	• 394	• 394	• 145+00	• 145+00	-2.266	• 394	
2.8	-2.762	-1.044	-1.396	• 396	• 396	• 145+00	• 145+00	• 396	-2.762	• 396	• 396	• 145+00	• 145+00	-2.762	• 396	• 396	• 145+00	• 145+00	-2.762	• 396	• 396	• 145+00	• 145+00	-2.762	• 396	• 396	• 145+00	• 145+00	-2.762	• 396	
3.0	-4.660	-2.402	-1.398	• 398	• 398	• 145+00	• 145+00	• 398	-4.660	• 398	• 398	• 145+00	• 145+00	-4.660	• 398	• 398	• 145+00	• 145+00	-4.660	• 398	• 398	• 145+00	• 145+00	-4.660	• 398	• 398	• 145+00	• 145+00	-4.660	• 398	
3.2	-5.460	-2.802	-1.347	• 347	• 347	• 145+00	• 145+00	• 347	-5.460	• 347	• 347	• 145+00	• 145+00	-5.460	• 347	• 347	• 145+00	• 145+00	-5.460	• 347	• 347	• 145+00	• 145+00	-5.460	• 347	• 347	• 145+00	• 145+00	-5.460	• 347	
3.4	-6.260	-3.202	-1.337	• 337	• 337	• 145+00	• 145+00	• 337	-6.260	• 337	• 337	• 145+00	• 145+00	-6.260	• 337	• 337	• 145+00	• 145+00	-6.260	• 337	• 337	• 145+00	• 145+00	-6.260	• 337	• 337	• 145+00	• 145+00	-6.260	• 337	
3.6	-7.061	-1.603	-1.337	• 337	• 337	• 145+00	• 145+00	• 337	-7.061	• 337	• 337	• 145+00	• 145+00	-7.061	• 337	• 337	• 145+00	• 145+00	-7.061	• 337	• 337	• 145+00	• 145+00	-7.061	• 337	• 337	• 145+00	• 145+00	-7.061	• 337	
3.8	-7.860	-2.002	1.398	• 398	• 398	• 145+00	• 145+00	• 398	-7.860	• 398	• 398	• 145+00	• 145+00	-7.860	• 398	• 398	• 145+00	• 145+00	-7.860	• 398	• 398	• 145+00	• 145+00	-7.860	• 398	• 398	• 145+00	• 145+00	-7.860	• 398	
4.0	-8.660	-2.802	1.347	• 347	• 347	• 145+00	• 145+00	• 347	-8.660	• 347	• 347	• 145+00	• 145+00	-8.660	• 347	• 347	• 145+00	• 145+00	-8.660	• 347	• 347	• 145+00	• 145+00	-8.660	• 347	• 347	• 145+00	• 145+00	-8.660	• 347	
4.2	-9.460	-3.202	1.337	• 337	• 337	• 145+00	• 145+00	• 337	-9.460	• 337	• 337	• 145+00	• 145+00	-9.460	• 337	• 337	• 145+00	• 145+00	-9.460	• 337	• 337	• 145+00	• 145+00	-9.460	• 337	• 337	• 145+00	• 145+00	-9.460	• 337	
4.4	-10.260	-3.202	1.337	• 337	• 337	• 145+00	• 145+00	• 337	-10.260	• 337	• 337	• 145+00	• 145+00	-10.260	• 337	• 337	• 145+00	• 145+00	-10.260	• 337	• 337	• 145+00	• 145+00	-10.260	• 337	• 337	• 145+00	• 145+00	-10.260	• 337	
4.6	-11.060	-3.202	1.337	• 337	• 337	• 145+00	• 145+00	• 337	-11.060	• 337	• 337	• 145+00	• 145+00	-11.060	• 337	• 337	• 145+00	• 145+00	-11.060	• 337	• 337	• 145+00	• 145+00	-11.060	• 337	• 337	• 145+00	• 145+00	-11.060</td		

EXACT ZIMM EIGENVALUES

EXACT ZIMM EIGENVALUES		N = 50		N = 050	
L1	LN	SUM	SUM	SUM(L1)	JFR
.525-n2	.365+n1	.274+n00	.339+n03	1.780	.562
		1/(LP)	L1/LP	ROCAL	(1/LP)2
		1/(LN)			(1/LP)12
					-23
					.928

REDUCED CYANAMIC VISCOSITY AND MODULUS

	MON	TUE	WED	THU	FRI	SAT	SUN	
LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG
DMT1	FTAIR	ETA2R	G1R	G2R	ETAIR	ETA2R	G1R	G2R
-2.8	-2.757	-5.557	-2.550	-1.784	-0.175	-0.278	-0.052	-0.282
-2.0	-2.50	-1.957	-3.957	-1.750	-1.784	-0.110	-0.01	-0.178
-1.8	-2.50	-1.757	-3.557	-1.550	-1.784	-0.175	-0.01	-0.277
-1.4	-2.50	-1.357	-2.757	-1.150	-1.784	-0.419	-0.01	-0.175
-1.0	-2.48	-1.961	-1.951	-0.752	-1.774	-0.109	-0.01	-0.177
-0.8	-2.44	-7.67	-1.567	-0.556	-1.754	-0.171	-0.00	-0.278
-0.6	-2.35	-0.581	-1.181	-0.765	-1.724	-0.263	-0.00	-0.659
-0.4	-2.15	-0.415	-0.915	-0.185	-1.644	-0.385	-0.00	-0.163
-0.2	-1.72	-0.287	-0.487	-0.028	-1.494	-0.516	-0.00	-0.326
0	-1.00	-0.222	-0.222	-0.100	-1.264	-0.599	-0.00	-0.126
2	-0.06	-0.224	-0.224	-0.024	-2.06	-1.014	-0.597	-0.946
4	-0.091	-0.267	-0.267	-0.133	-3.09	-8.114	-0.100	-1.161
6	-0.186	-0.326	-0.326	-0.274	-4.14	-6.524	-0.070	-2.044
8	-0.282	-0.393	-0.393	-0.477	-5.18	-5.234	-0.050	-2.205
0	-0.379	-0.466	-0.466	-0.534	-6.21	-4.184	-0.030	-1.034
2	-0.477	-0.544	-0.544	-0.656	-7.23	-3.334	-0.010	-1.264
4	-0.577	-0.624	-0.624	-0.776	-8.23	-2.654	-0.000	-1.264
6	-0.680	-0.706	-0.706	-0.894	-9.20	-2.094	-0.000	-1.974
8	-0.787	-0.788	-0.788	-1.012	-1.013	-1.634	-0.000	-1.254
0	-0.859	-0.870	-0.870	-1.130	-1.101	-1.264	-0.000	-1.350
2	-2-1.023	-0.950	-1.250	-1.177	-1.250	-1.229	-0.229	-1.268
4	-4-1.66	-1.032	-1.032	-1.032	-1.032	-1.032	-0.000	-1.032
6	-6-1.343	-1.121	-1.121	-1.479	-1.479	-1.479	-0.000	-1.479
8	-8-1.571	-1-229	-1-229	-1.571	-1.571	-1.571	-0.000	-1.571
3	-8-1.571	-1-229	-1-229	-1.571	-1.571	-1.571	-0.000	-1.571
5	-8-3.355	-2.103	-1.697	-0.445	-0.445	-0.445	-0.000	-0.445
4	-2-4.153	-2.501	-1.699	-0.047	-0.047	-0.047	-0.000	-0.047
6	-6-4.952	-2.901	-1.699	-0.352	-0.352	-0.352	-0.000	-0.352
5	-0-5.752	-3.301	-1.699	-0.752	-0.752	-0.752	-0.000	-0.752

EXACT ZIMM EIGENVALUES
 L_1 L_N $1/(LN)$
 .598 -n2 • 348•01 • 287•00

EXACT ZIMM EIGENVALUES

L1	L _N	1/(LN)	SUM	RECIP	SUM	SUM(L1)	JER	PHI
1/(LP)	1/LP	1/LP	1/LP	ROCAL	(1/LP) ^{1/2}	(LP) ^{1/2}		-23
• 308+03	1.840	• 543	• 312+05	1.1139	• 329	1.265		
• 348+01	• 287+00							
• 598-02								
							N = 50	H = .075

SHINING A NEW LIGHT ON PRODUCED WATER

EXACT ZIMM EIGENVALUES
 $L_1 \quad \ln(1/LN)$ SUM $1/(LP)$ RECIP $(1/(LP))^2$ SUM $(LP)^2$ PHI
 $-669.02 + 331.01i \cdot 302 + 00$ $283 + 03$ $1.898 - 527i$ $250 + 05$ $1.1221 + 312i - 552i$

REDUCED DYNAMIC VISCOSITY AND MODULUS									
LOG	LOG	LOG	LOG	LOG	SUM	RECIP	SUM	SUM(L1)	JFR
OWT1	ETA1R	ETA2R	G1R	G2R	ETA1R	ETA2R	G1R	G2R	PHI
-2.8	+278	-2.750	-5.550	-2.522	-190+01	178-02	-282-05	-301-02	-190+01 • 937-03
-2.0	+278	-1.950	-3.950	-1.722	-190+01	112-01	-112-01	-190+01	-190+01 • 591-02
-1.8	+278	-1.750	-3.550	-1.522	-190+01	178-01	-282-03	-301-01	-190+01 • 937-02
-1.4	+278	-1.351	-2.751	-1.122	-190+01	44-01	-178-02	-755-01	-190+01 • 235-01
-1.0	+276	-954	-1.954	-724	-189+01	111+00	-111+01	189+00	-189+01 • 589-01
-0.8	+272	-760	-1.560	-528	-187+01	174+00	-276-01	297+00	-188+01 • 926-01
-0.6	+264	-574	-1.174	-336	-184+01	267+00	-670-01	461+00	-186+01 • 144+00
-0.4	+245	-407	-807	-155	-176+01	392+00	-156+00	699+00	-180+01 • 219+00
-0.2	+205	-279	-479	-805	-160+01	526+00	-322+00	101+01	-169+01 • 318+00
0.0	+137	-211	-211	-211	-137+01	615+00	-915+00	137+01	-150+02 • 42+00
0.2	+050	-208	-208	-250	-112+01	619+00	-981+00	178+01	-128+01 • 504+00
0.4	-041	-245	-155	-359	-910+00	569+00	-143+01	229+01	-107+01 • 612+00
0.6	-131	-298	-302	-469	-740+00	564+00	-201+01	294+01	-895+00 • 598+00
0.8	-222	-359	-441	-578	-599+00	438+00	-276+01	378+01	-168+02 • 931+00
1.0	-316	-426	-574	-684	-483+00	375+00	-375+01	483+01	-687+00 • 687+00
1.2	-411	-497	-703	-789	-288+00	318+00	-505+01	615+01	-321+03 • 791-02 • 499+02 • 202+01
1.4	-509	-571	-879	-891	-309+00	268+00	-674+01	777+01	-168+02 • 216+00 • 168+02 • 900+00
1.6	-612	-546	-954	-988	-245+00	226+00	-899+01	971+01	-112+02 • 460+02 • 112+02 • 473+01 • 133+01
1.8	-720	-722	-1078	-1080	-191+00	190+00	-120+02	120+02	-269+00 • 781+00
2.0	-838	-797	-1202	-1162	-145+00	150+00	-150+02	145+02	-216+00 • 833+00
2.2	-673	-873	-1327	-1227	-106+00	134+00	-212+02	168+02	-171+00 • 900+00
2.4	-1139	-955	-1445	-1261	-727-01	111+00	-278+02	183+02	-133+00 • 900+00
2.6	-1351	-1.054	-1546	-1249	-446-01	893-01	-352+02	178+02	-99+01 • 110+00
2.8	-494	-2.102	-1.619	-1.177	-238-01	1.177	-791-02	99+01	-197-01 • 147+01
3.0	-1.951	-1.338	-1.049	-1.261	-1.049	-1.049	-460+01	460+01	-101-01 • 122+01 • 122+01
3.4	-7.702	-1.707	-1.693	-1.693	-1.693	-1.693	-196-01	196-01	-499+01 • 147+01
3.8	-3.494	-2.102	-1.698	-1.698	-1.698	-1.698	-306	-306	-791-02 • 153+01
4.2	-4.292	-2.501	-1.699	-1.699	-0.92	510-04	-315-02	500+02	-809+00 • 315-02 • 155+01
4.6	-5.092	-2.901	-1.699	-1.699	-4.92	-809-05	-126-02	-322+00	-126-02 • 156+01
5.0	-5.82	-3.301	-1.699	-1.699	-892	-128-05	-500+02	-128+00	-500+00 • 300+02 • 128+00 • 500+00

EXACT ZIMM EIGENVALUES
 L1 LN 1/ILNI
 • 755-02 • 311+01 • 322+00

N = 50	H0 = 130	
SUM(L1)	JER	PHI
/LP12		-23
2		
5	1.1309	•293 1.851

SOCIETY FOR ADVANCED CYBERNETICS

• 812-02 • 297+01 • 337+00
EXACT ZIMM EIGENVALUES
L1 LN 1/LN)

EXACT ZIMM EIGENVALUE'S		$N = 50$		$N = 150$	
L_1	\ln	SUM	RECIP	SUM	RECIP
1/(LN)	1/(LN)	1/(LP)	ROCAL	SUM(LP)	JER
.812-02	.297+01	.337+00	.247+03	.499	.172+05
					1.1362
					.282
					2.029
					-23

MOHURRAS AND CYANAMIC VISCOSEITY

EXACT ZIMM EIGENVALUES
L1 LN 1/(LN)
.953-02 • 263+01 • 380+00

	RECIP	SUM ^{LP}	SUM(L1)	JEP	PHI
ROCAL	(1/LP)2	/LP)2			-23
2.110	.474	.126+05	1.1492	.258	2.474
				N = 50	H = .20

REDUCED DYNAMIC VISCOSITY AND MODULUS

-60-

#1250

EXACT ZIMM EIGENVALUES
 $L_1 \ln 1/(LN)$
 $.109-01 \cdot 229+01 \cdot 437+00$

EXACT ZIMM EIGENVALUES				N=50 H*=250			
L1	LN	1/(LN)	SUM	SUM	SUM(L1)	JER	PHI
1.09-0.01	-229+0.01	437+0.00	•203+0.03	2.215	•452	•969+0.04	1.1587
				RECIP	ROCAL	(1/LP)12	/LP12
				L1/LP			

MOGULUS AND VISCOELASTIC BEHAVIOR

EXACT ZIMM EIGENVALUES
L1 LN 1/(LN)

SUM	SUM	RECIP	SUM	SUM(LL)	JFR	PHI
1/(LP)	L1/LP	ROCAL	(1/LP) ²	(LP) ²		-23
•199+03	2.241	•446	•914+04	1.1611	•231	2.853

REDUCED DYNAMIC VISCOSITY AND

EXACT ZIMM EIGENVALUES
11 LN 1/LN)
•123-01 •195+01 •514+00

	SUM	SUM(L1)	JER	• 30
(1/LP) ²	/LP) ²			-23
• 769•04	1•1684	• 216		3•101

REFINED DYNAMIC VISCOSITY AND MODULUS

•157-52 •366•01 •273•00
L1 TIN EIGENVALUES
EXIT ZIMM

	RECIP	SUM	N=100	H= .05	FHI
SUM		SUM(L1)	JFR		
L1/LP	FOCAL	(1/LP)2	/LP)2		-23
1.821	.549	.450+.06	1.1099	.3335	.123.

מִשְׁנָה בְּבֵית הַדָּת אֶנְצֹלָחָה

EXACT ZIMM EIGENVALUES
 L_1 \ln $1/(LN)$
 $1.187 - i 2.349 \pm 01.287 + 00$

RECIP	SUM	SUM(L)	JER	PHI
LOCAL	(1/LP)2	1/LP12		-23
L1/LP	1.891	.529		
SUM	N=100	H=-.075		
			313	1.466
			321.005	1.1196

REDUCED DYNAMICS VISCOSITY AND MOULUS

• 2017-02 • 331 • 01 • 302 • 000
EXACT ZIMM EIGENVALUES
LN LN

SUM	RECIP	SUM	SUM(LL)	JER	PHI
L1/LP	ROCAL	(1/LP) ^{1/2}	/LP) ^{1/2}	-23	
1.953	.512	.2470406	1.12776	.296	1.746

REDUCED DYNAMIC VISCOSITY AND MODULUS

EXACT ZIMM EIGENVALUES

L1	LN	1/(LN)	SUM	SUM	RECIP	SUM	L1/LP	ROCAL	L1/LP(1/2)	L1/LP(2)	179+06 1.0.1355	• 278	2.0.19
• 252-02	• 311+01	• 322+00	• 802+03	2.0.21	• 495	• 179+06 1.0.1355	• 278	2.0.19					

N=100 H=-130

REDUCED CYANAMIC VISCOOSITY AND MODULUS

LOG LOG													
0.111	E7A1R	E7A2R	E7A1P	E7A2P	E7A1R	E7A2R	E7A1P	E7A2P	E7A1R	E7A2R	E7A1P	E7A2P	E7A1R
-2.8	-306	-2.745	-5.545	-1.345	-2.745	-1.345	-1.345	-1.345	-1.345	-1.345	-1.345	-1.345	-1.345
-1.8	-306	-1.745	-1.494	-1.494	-1.494	-1.494	-1.494	-1.494	-1.494	-1.494	-1.494	-1.494	-1.494
-2.0	-306	-1.945	-3.545	-3.545	-3.545	-3.545	-3.545	-3.545	-3.545	-3.545	-3.545	-3.545	-3.545
-1.0	-303	-0.949	-1.949	-1.949	-1.949	-1.949	-1.949	-1.949	-1.949	-1.949	-1.949	-1.949	-1.949
-0.8	-300	-0.754	-1.554	-1.554	-1.554	-1.554	-1.554	-1.554	-1.554	-1.554	-1.554	-1.554	-1.554
-1.0	-203	-0.237	-0.237	-0.237	-0.237	-0.237	-0.237	-0.237	-0.237	-0.237	-0.237	-0.237	-0.237
-0.0	-174	-0.174	-0.174	-0.174	-0.174	-0.174	-0.174	-0.174	-0.174	-0.174	-0.174	-0.174	-0.174
-0.2	-124	-0.093	-0.093	-0.093	-0.093	-0.093	-0.093	-0.093	-0.093	-0.093	-0.093	-0.093	-0.093
-0.6	-57	-0.040	-0.040	-0.040	-0.040	-0.040	-0.040	-0.040	-0.040	-0.040	-0.040	-0.040	-0.040
-0.8	-16	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018	-0.018
-0.2	-82	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.4	-426	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.6	-174	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.8	-974	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.2	-335	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.4	-737	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.6	-396	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.8	-119	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.2	-918	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.4	-518	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.6	-147	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.8	-518	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.2	-929	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.4	-245	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.6	-1071	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.8	-225	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.2	-8125	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.4	-1057	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.6	-1743	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.8	-977	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.2	-610	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.4	-1551	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.6	-1546	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.8	-154	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.2	-101	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.4	-257	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.6	-610	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
-0.8	-1999	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000

EXACT ZINN EIGENVALUES
 L1 LN 1/(LN)
 .276-0.2 • 297+01 • 336+00

RECIP	SUM	N=100	H= .15
ROCAL	(1/p) ²	1.1401	.268
L1,p	(1/p) ²	1.1401	2.175
RECIP	SUM	0.484	2.064

REDUCED SYMMETRY

• 3.34 - 0.2 • 263.01 • 380.00
EXACT ZIMM EIGENVALUES
L1 LN 1/1(N)

EXACT ZIMM EIGENVALUES		N=100		N=20	
L1	LN	SUM	RECIP	SUM	SUM(LP)
1/(LN)	1/(LP)	L1/LP	ROCAL	(1/LP) ²	JER PHI
•334-022	•263+01	•380+00	•548+03	•462	-23
		2.165		•103+06	1.1496 •245 2.509

PREDUCED DYNAMIC ECOLOGICAL SISCOMICITY AND MIGRATION

LOG	L-G LOG			LOG			LOG			LOG			LOG			MON				
	0MTI	ETAI R	ETAI R	61R	62R	62R	61R	ETAI R	ETAI R	GIR	ETAI R	GIR	ETAI R	G2R	ETAR	ETAR				
-2.8	-2.0	-3.5	-1.9	-2.7	-3.9	-5.5	-3.9	-2.4	-4.6	-5.5	-2.1	-1.9	-2.0	-3.4	-3.0	-842-03				
-2.0	-2.0	-3.5	-1.9	-2.7	-3.9	-5.5	-3.9	-1.6	-6.6	-5.5	-2.1	-1.5	-0.3	-2.1	-0.1	-531-02				
-1.8	-1.8	-3.5	-1.7	-2.4	-3.0	-5.4	-3.0	-1.4	-6.5	-5.5	-2.1	-1.8	-2.0	-3.4	-0.1	-842-02				
-1.4	-1.4	-3.5	-1.3	-3.4	-2.0	-7.4	-0.6	-1.0	-6.5	-5.5	-2.1	-4.5	-7.0	-1.8	-0.1	-211-01				
-1.0	-1.0	-3.3	-0.9	-4.3	-1.9	-9.4	-1.9	-0.6	-6.7	-5.5	-2.1	-5.0	-1.0	-0.1	-0.1	-528-01				
-0.8	-0.8	-3.0	-0.7	-7.49	-1.54	-9.59	-0.74	-0.7	-4.70	-4.01	-1.78	-0.00	-2.83	-0.01	-0.1	-831-01				
-0.6	-0.6	-3.2	-0.5	-6.3	-1.16	-13.0	-2.77	-0.94	-2.77	-2.01	-2.74	-0.00	-6.87	-0.01	-0.1	-129+06				
-0.4	-0.4	-3.06	-0.3	-9.5	-0.79	-9.5	-0.94	-0.20	-2.02	-0.01	-4.03	-0.00	-1.60	-0.00	-0.0	-206+01				
-0.2	-0.2	-2.71	-0.2	-2.65	-0.45	-4.55	-0.07	-1.87	-0.71	-1.87	-0.01	-5.43	-0.00	-3.43	-0.00	-0.0	-196+00			
0	0	-2.13	-0	-1.94	-0.194	-1.94	-2.13	-0.163	-1.94	-0.194	-0.194	-0.01	-1.78	-0.00	-2.15	-0.01	-0.0	-196+00		
2	2	-1.84	-0	-1.84	-0.184	-1.84	-0.184	-0.16	-1.84	-0.184	-0.184	-0.01	-1.78	-0.00	-2.12	-0.01	-0.0	-196+00		
4	4	-0.60	-0	-2.11	-1.89	-1.89	-4.60	-1.15	-0.61	-1.89	-1.89	-0.01	-1.54	-0.01	-1.30	-0.01	-0.0	-196+00		
6	6	-0.017	-0	-2.54	-0.346	-2.54	-5.83	-0.961	-0.557	-2.54	-0.346	-0.01	-2.22	-0.01	-3.83	-0.01	-0.0	-196+00		
8	8	-0.096	-0	-3.05	-4.95	-3.05	-7.04	-8.02	-4.95	-3.05	-4.95	-0.00	-4.96	-0.00	-3.13	-0.01	-0.0	-196+00		
10	10	-0.176	-0	-3.61	-6.39	-3.61	-8.24	-6.66	-6.39	-3.61	-8.24	-0.00	-4.36	-0.01	-6.66	-0.01	-0.0	-196+00		
12	12	-0.259	-0	-4.21	-7.79	-4.21	-9.41	-5.51	-7.79	-4.21	-9.41	-0.00	-3.80	-0.00	-6.02	+0.01	-0.0	-196+00		
14	14	-0.344	-0	-4.83	-9.17	-4.83	-10.55	-4.53	-9.17	-4.83	-9.17	-0.00	-8.26	-0.01	-11.4	-0.02	-0.0	-196+00		
16	16	-0.432	-0	-5.47	-1.053	-5.47	-1.053	-1.068	-3.70	-0.547	-1.053	-1.053	-0.00	-2.94	-0.00	-1.13	-0.02	-0.0	-196+00	
18	18	-0.525	-0	-6.11	-1.189	-6.11	-1.189	-1.275	-2.98	-0.525	-1.189	-1.189	-0.00	-2.45	-0.00	-1.55	-0.02	-0.0	-196+00	
20	20	-0.625	-0	-6.74	-1.326	-6.74	-1.326	-1.375	-2.37	-0.625	-1.326	-1.326	-0.00	-2.12	-0.00	-2.37	-0.02	-0.0	-196+00	
22	22	-0.726	-0	-7.38	-1.462	-7.38	-1.462	-1.464	-1.84	-0.726	-1.462	-1.462	-0.00	-1.83	-0.00	-2.90	-0.02	-0.0	-196+00	
24	24	-0.865	-0	-8.02	-1.598	-8.02	-1.598	-1.535	-1.37	-0.865	-1.598	-1.598	-0.00	-1.58	-0.00	-3.96	-0.02	-0.0	-196+00	
26	26	-1.024	-0	-8.74	-1.726	-8.74	-1.726	-1.576	-9.46	-0.1	-1.726	-1.726	-0.00	-1.34	-0.00	-5.32	-0.02	-0.0	-196+00	
28	28	-1.232	-0	-9.64	-1.836	-9.64	-1.836	-1.568	-5.96	-0.1	-1.836	-1.836	-0.00	-1.09	-0.00	-6.95	-0.02	-0.0	-196+00	
30	30	-1.502	-1	-0.85	-1.915	-0.85	-1.915	-1.498	-3.15	-0.1	-1.915	-1.915	-0.00	-8.21	-0.01	-8.21	-0.02	-0.0	-196+00	
32	32	-2.193	-1	-4.17	-1.993	-4.17	-1.993	-1.207	-6.41	-0.2	-1.993	-1.993	-0.00	-3.93	-0.01	-9.62	-0.02	-0.0	-196+00	
34	34	-8.2972	-1	-8.03	-1.997	-8.28	-1.997	-1.07	-1.57	-0.1	-8.28	-8.28	-0.00	-4.32	-0.02	-6.30	-0.02	-0.0	-196+00	
36	36	-4.567	-2	-6.00	-2.000	-6.00	-2.000	-0.33	-2.71	-0.4	-2.000	-2.000	-0.00	-1.98	-0.01	-2.51	-0.02	-0.0	-196+00	
38	38	-5.367	-3	-3.000	-2.000	-3.000	-2.000	-0.00	-3.67	-4.29	-0.5	-3.000	-3.000	-0.00	-4.29	-0.00	-1.00	-0.02	-0.0	-196+00

EXACT ZIMM EIGENVALUES

• 25

EXACT ZIMM EIGENVALUES
 L_1 $\ln L_1 / \langle L \rangle N$ SUM
 $1/(LP)$ L_1/LP $RECIP$
 $.576+03$ $.576+03$ $ROCAL$
 $.392-02$ $.229+01$ $4.37+00$

REDUCED DYNAMIC VISCOSITY AND MODULUS

EXACT ZIMM EIGENVALUES
L1 LN 1/(LN)
.406 - .02 • .221 + .01 • .453 + .00

	SUM	SUM(L1)	JER	L1/P12	L1/P12	05/04/2017	05/04/2017	1.1589	• 222	2.8552
N=1100	M=• 262							-23		

REFINED DYNAMIC VISCOSITY AND MODULUS

EXACT ZIMM EIGENVALUES
 L_1 $\ln \lambda_1$ $1/(L_1)$
 $L_1/(LP)$ $524+03$ 2.360 424
 $50-02$ $195+01$ $514+00$

N=100 H*= .30
 L_1/LP $574+05$ 1.1636 $.209$ 3.044
 L_1/LP $574+05$ 1.1636 $.209$ 3.044

REDUCED DYNAMIC VISCOSITY AND MODULUS

LOG LOG	LOG LOG	SUM	RECIP	SUM	JER	PHI	ARCTAN
0MTI	FTAIR	ETA2R	619	62R	ETAIR	61R	62R
-2.8	-373	-2.734	-5.534	-2.427	-236+01	194-02	292-05
-2.0	-373	-1.934	-3.934	-1.627	-236+01	116-01	236+01
-1.8	-373	-1.734	-3.534	-1.427	-236+01	184-01	292-03
-1.4	-373	-1.335	-2.735	-1.027	-236+01	463-01	374-01
-1.0	-371	-938	-1.938	-6.629	-235+01	115+00	115-01
-0.8	-368	-744	-1.544	-4.32	-233+01	180+00	286-01
-0.6	-361	-557	-1.157	-2.39	-230+01	277+00	696-01
-0.4	-346	-389	-789	-0.54	-222+01	408+00	162+00
-0.2	-314	-258	-458	-1.14	-206+01	552+00	348+00
0	-261	-185	-185	-2.61	-182+01	653+00	133+01
0.2	-194	-172	-172	-3.94	-156+01	674+00	107+01
0.4	-124	-194	-194	-524	-133+01	639+00	234+01
0.6	-055	-231	-369	-655	-113+01	598+00	161+01
0.8	-015	-274	-526	-785	-956+00	532+00	326+01
1.0	-087	-322	-678	-913	-819+00	477+00	477+01
1.2	-161	-371	-829	-1.039	-691+00	426+00	109+01
1.4	-238	-420	-990	-1.162	-578+00	380+00	954+01
1.6	-320	-469	-1.131	-1.280	-478+00	340+00	110+01
1.8	-410	-516	-1.284	-1.390	-399+00	305+00	193+02
2.0	-513	-561	-1.439	-1.487	-307+00	275+00	207+02
2.2	-638	-608	-1.592	-1.562	-230+00	246+00	365+02
2.4	-801	-668	-1.732	-1.599	-158+00	215+00	540+02
2.6	-1.020	-753	-1.847	-1.580	-956-01	177+00	703+02
2.8	-1.303	-876	-1.924	-1.497	-497-01	133+00	839+02
3.0	-1.641	-1.034	-1.956	-1.359	-229-01	925+02	925+02
3.4	-4.01	-1.406	-1.994	-0.999	-397-02	193-01	987+02
3.6	3.194	-1.801	-1.999	-6.06	-640-03	158-01	998+02
4.0	-3.993	-2.200	2.000	-207	-102-03	631-02	100+03
4.6	-7.792	-2.600	2.000	-1.92	-161-04	251-02	100+03
5.0	-5.592	-3.000	2.000	-0.592	-256-05	100-02	100-02
						100+03	256+00

EXACT ZIMM EIGENVALUES
 L_1 $\ln(1/L_1)$ \sum \sum RECIP
 $1/ILP_1$ $1/ILP_2$ $ROCAL$ $(1/ILP_1)^2$ ILP_2 PHI
 $-4.79 - 0.3 \cdot 366 + 0.1 \cdot 273 + 0.0 \cdot 390 + 0.4 \cdot 866 + 0.536 \cdot 487 + 0.7 \cdot 1.157 \cdot 321 \cdot 1.334$

N=200 H=-.05
 L_1 $\ln(1/L_1)$ \sum \sum RECIP
 $1/ILP_1$ $1/ILP_2$ $ROCAL$ $(1/ILP_1)^2$ ILP_2 PHI
 $-2.3 \cdot 321 \cdot 1.334$

REDUCED LOG		DYNAMIC LOG		VISCOSITY LOG		IND MODULUS		MOD	
OHT	ETAIR	ETA2R	G1R	G2R	ETAIR	ETA2R	G1R	ETAIR	ETA2R
-2.8	+271	-2.752	-5.552	-2.529	-187+01	-177+02	-280+05	-296+02	-187+01
-2.0	+271	-1.952	-3.952	-1.729	-187+01	-112+01	-112+03	-187+01	-187+01
-1.8	+271	-1.753	-3.553	-1.529	-187+01	-177+01	-280+03	-296+01	-187+01
-1.4	+270	-1.353	-2.753	-1.130	-186+01	-444+01	-177+02	-742+01	-186+01
-1.0	+268	-0.956	-1.956	-0.732	-186+01	-111+00	-111+01	-186+00	-186+01
-0.8	+265	-0.762	-1.562	-0.535	-184+01	-173+00	-274+01	-292+00	-195+01
-0.6	+256	-0.576	-1.176	-0.346	-180+01	-265+00	-666+01	-453+00	-192+01
-0.4	+237	-0.410	-0.810	-0.163	-172+01	-389+00	-155+00	-687+00	-177+01
-0.2	+196	-0.282	-0.482	-0.074	-157+01	-523+00	-330+00	-991+00	-165+01
0	+127	-0.215	-0.215	-0.127	-134+01	-609+00	-609+00	-134+01	-147+01
2	+039	-0.214	-0.014	+239	-109+01	-511+00	-968+00	-173+01	-125+01
4	+053	-0.253	+147	+347	-885+00	-558+00	-140+01	-222+01	-105+01
6	+144	+309	+291	+456	-718+00	-691+00	-196+01	-286+01	-396+00
8	+235	+372	+428	+565	-582+00	-424+00	-268+01	-367+01	-630+00
10	+327	+413	+557	+673	-471+00	-361+00	-361+01	-471+01	-593+00
12	+421	+519	+981	+779	-380+00	-303+00	-480+01	-602+01	-105+01
14	+515	+598	+802	+885	-306+00	-252+00	-634+01	-768+01	-563+00
16	+610	+680	+920	+960	-296+00	-209+00	-811+01	-978+01	-654+00
18	+705	+765	+1035	+1095	-197+00	-172+00	-108+02	-124+02	-261+00
20	+802	+851	+149	+1198	-158+00	-141+00	-141+02	-158+02	-211+00
22	+901	+938	+1262	+1293	-126+00	-115+00	-183+02	-196+02	-171+00
24	+1000	+1026	+1374	+1400	-92+01	-237+02	-237+02	-251+02	-137+00
26	+102	+114	+1486	+1498	-790+01	-770+01	-306+02	-315+02	-772+00
28	+208	+200	+1600	+1592	-620+01	-630+01	-388+02	-391+02	-884+01
30	+319	+286	+1714	+1681	-480+01	-518+01	-518+02	-480+02	-706+01
32	+41577	+452	+1948	+823	-265+01	-353+01	-887+02	-665+02	-441+01
34	+1.960	+643	+2157	+840	-110+01	-227+01	-143+03	-691+02	-252+01
36	+2.567	+933	+2267	+1633	-271+02	-117+01	-185+03	-430+02	-120+01
38	+3.320	+305	+2295	+1280	-479+03	-46+02	-197+03	-191+02	-498+02
40	+4.111	+700	+2300	+889	-774+04	-200+02	-200+03	-774+01	-200+02
42	+5.334	+01	+01	+01	+01	+01	+01	+01	+01

ARCTAN
 L_1 $\ln(1/L_1)$ \sum \sum RECIP
 $1/ILP_1$ $1/ILP_2$ $ROCAL$ $(1/ILP_1)^2$ ILP_2 PHI
 $-2.3 \cdot 321 \cdot 1.334$

MOD
 L_1 $\ln(1/L_1)$ \sum \sum RECIP
 $1/ILP_1$ $1/ILP_2$ $ROCAL$ $(1/ILP_1)^2$ ILP_2 PHI
 $-2.3 \cdot 321 \cdot 1.334$

EXACT ZIMM EIGENVALUES
L1 LNE /LN1
-594-03 -349+01 -287+00

EXACT ZIMM EIGENVALUES		N=200		N=075	
L1	LN	SUM	SUM	SUM(L1)	JER
1/(LN)	1/(LP)	L1/LP	ROCAL	(1/(LP)) ²	PHI
•594-03	-349+01	•287+00	•327+04	•515	-23
				•319+07	1.1251
					•299
					1.677

PREDICTION OF VISCOSITY AND SHEAR THICKNESS

EXACT ZIMM EIGENVALUES		N=200		N=075	
L1	LN	SUM	SUM	SUM(L1)	JER
1/(LN)	1/(LP)	L1/LP	ROCAL	(1/(LP)) ²	PHI
•594-03	-349+01	•287+00	•327+04	•515	-23
				•319+07	1.1251
					•299
					1.677

EXACT ZIMM EIGENVALUES		N=200		N=075	
L1	LN	SUM	SUM	SUM(L1)	JER
1/(LN)	1/(LP)	L1/LP	ROCAL	(1/(LP)) ²	PHI
•594-03	-349+01	•287+00	•327+04	•515	-23
				•319+07	1.1251
					•299
					1.677

•710-03 •332+01 •302+00
EXACT ZIMM EIGENVALUES
L1 LN 1/(LN)

N=200	H=	.10	
SUM	SUM(L1)	JFR	PHI
(1/LP12)	(LP12	-23	
.225+07	1.1326	.282	1.934

הבדלים בין דינמי ועכשווי וינם מודדים

MOD									
LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG
OMT1	ETA1R	ETA2R	G1R	G2R	ETA1R	ETA2R	G1R	ETA2R	G2R
-2.8	+302	-2.746	-5.546	-2.493	+201+01	-180-02	+284-05	+318-C2	+201+01
-2.0	+302	-1.946	-3.946	-1.698	+201+01	-113-01	+201-n1	+201-01	-565-02
-1.8	+302	-1.746	-3.546	-1.498	+201+01	-179-01	+284-03	+318-n1	+895-02
-1.4	+302	-1.347	-2.747	-1.098	+200+01	+450-01	+179-02	+798-n1	+225-01
-1.0	+300	-0.950	-1.950	-0.700	+200+01	+112+01	+200+00	+200+01	+562-01
-0.8	+297	-0.756	-1.556	-0.503	+198+01	+176+00	+278-01	+314+00	+199+01
-0.6	+289	-0.570	-1.170	-0.311	+194+01	+269+00	+677-01	+488+00	+196+01
-0.4	+270	-0.402	-0.802	-0.130	+186+01	+396+00	+158+00	+742+00	+191+01
-0.2	+233	-0.273	-0.473	+0.33	+171+n1	+533+00	+336+00	+108+01	+179+01
0	+169	-0.204	-0.204	+0.169	+148+01	+625+00	+625+00	+148+01	+160+01
2	+088	-0.199	-0.199	+0.001	+288	+122+01	+633+00	+100+01	+194+01
4	+003	-0.232	-0.168	+0.03	+101+01	+586+00	+147+01	+253+n1	+116+01
6	-0.081	-0.281	+0.319	+0.519	+830+00	+523+00	+208+n1	+330+n1	+981+00
8	-0.166	-0.339	+0.461	+0.634	+682+00	+458+00	+289+n1	+430+01	+822+00
0	-0.252	-0.403	+0.597	+0.748	+559+00	+395+00	+395+n1	+559+n1	+685+00
2	-0.340	-0.472	+0.728	+0.860	+457+0n1	+337+00	+337+n1	+724+01	+56A+n1
4	-0.429	-0.545	+0.855	+0.971	+372+00	+295+00	+716+n1	+935+n1	+469+00
6	-0.519	-0.620	+0.980	+1.081	+302+00	+240+00	+954+01	+120+02	+120+00
8	-0.611	-0.698	+1.102	+1.189	+245+00	+200+00	+126+n2	+154+02	+316+00
0	-0.705	-0.778	+1.222	+1.295	+197+n0	+167+n0	+167+n2	+197+n2	+258+00
2	-0.801	-0.858	+1.342	+1.399	+158+00	+139+00	+220+02	+251+02	+210+00
4	-0.899	-0.939	+1.451	+1.501	+126+00	+115+00	+289+02	+317+n2	+171+00
6	-1.002	-1.019	+1.591	+1.598	+995-n1	+957-01	+381+n2	+396+n2	+138+00
8	-1.111	-1.098	+1.702	+1.689	+774-n1	+798-01	+503+n2	+489+n2	+111+00
0	-1.230	-1.176	+1.824	+1.770	+588-01	+667-01	+667+n2	+588+n2	+889-01
2	-1.538	-1.339	+2.061	+1.862	+230-n1	+458-01	+115+n3	+729+n2	+542-01
4	-1.572	+2.228	+1.764	+921-02	+268-01	+169+n3	+169+n3	+581+n2	+283-01
6	-2.036	+1.572	+2.287	+1.462	+183-02	+122-01	+194+n3	+290+n2	+124-01
8	-2.316	+2.301	+1.281	+1.081	+303-03	+500-02	+199+n3	+120+n2	+151+01
0	-2.699	+2.301	+1.299	+1.081	+483-04	+200-02	+200+n3	+483+n1	+200-02

EXACT ZIMM EIGENVALUES
L1 LN 1/1161
•849-03 •311-01 •322-00

EXACT ZIMM EIGENVALUES		N=200		N=130				
L1	LN	SUM 1/(LN)	SUM 1/(LP)	RECIP ROCAL	SUM SUM(L1) (1/LP)12 •15A+07	SUM JER (LP)12 1.1397	PHI -2.3 •265	•1.130
.849-0.3	*311+01	*322+00	.244+04	2.074	.482			2.175

MODIFIED BYMATE VISCOSESTY AND MODIFIES

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L06	LOG	LOC	L05	ETA1R	ETA2R	G1R	G2R	ETA1R	ETA2R	G1R	G2R	ETA1R	ETA2R	G1R	G2R	
DMT1	DMT1	LOC	DMT1	-2.8	• 317	-2.743	-5.543	-2.483	• 207+01	-181-02	• 286-05	• 329-02	• 207+01	• 871-03	• 207+01	• 871-02
-2.8	• 317	-1.943	-3.943	-1.693	• 207+01	-114-01	-114-01	-114-01	• 207-01	-207-01	• 207-03	• 207-01	• 207-01	• 549-02	• 207-01	• 549-02
-2.0	• 317	-1.743	-3.543	-1.483	• 207+01	-181-01	-286-03	-286-03	• 207-01	-207-01	• 207-03	• 207-01	• 207-01	• 871-02	• 207-01	• 871-02
-1.8	• 317	-1.344	-2.744	-1.084	• 207+01	-453-01	-180-02	-180-02	• 207-01	-207-01	• 825-01	• 207-01	• 207-01	• 219-01	• 207-01	• 219-01
-1.4	• 316	-0.947	-1.947	-0.685	• 206+01	-113-00	-113-00	-113-00	• 206+00	• 206+00	• 206+00	• 206+00	• 206+01	• 547-01	• 206+01	• 547-01
-1.0	• 315	-0.753	-1.553	-0.489	• 205+01	-177+00	-280-01	-280-01	• 205+00	• 205+00	• 325+00	• 206+01	• 206+01	• 860-01	• 206+01	• 860-01
-0.8	• 314	-0.567	-1.157	-0.295	• 201+01	-271+00	-681-01	-681-01	• 201+00	• 271+00	• 506+00	• 203+01	• 203+01	• 134+00	• 203+00	• 134+00
-0.6	• 304	-0.399	-0.799	-0.114	• 193+01	-399+00	-159+00	-159+00	• 193+00	• 399+00	• 769+00	• 197+01	• 197+01	• 203+00	• 197+01	• 203+00
-0.4	• 286	-0.250	-0.470	-0.050	• 178+01	-57+00	-339+00	-339+00	• 178+00	• 57+00	• 112+01	• 186+01	• 186+01	• 294+00	• 186+01	• 294+00
-0.2	• 250	-0.200	-0.200	-0.000	• 168	-154+01	-631+00	-631+00	• 168	-154+01	-154+01	• 167+01	• 167+01	• 388+00	• 167+01	• 388+00
0	• 188	-0.000	-0.000	-0.000	• 310	-129+01	-642+00	-642+00	• 310	-129+01	-102+01	• 204+01	• 204+01	• 462+00	• 204+01	• 462+00
2	• 110	-0.193	-0.007	-0.007	• 429	-107+01	-598+00	-598+00	• 429	-107+01	-150+01	• 258+01	• 258+01	• 510+05	• 222+01	• 510+05
4	• 029	-0.223	-0.223	-0.223	• 330	-548	-896+00	-896+00	• 330	-537+00	-214+01	• 353+01	• 353+01	• 545+00	• 104+01	• 545+00
6	-0.052	-0.270	-0.270	-0.270	• 475	-666	-734+00	-734+00	• 475	-666	-299+01	• 463+01	• 463+01	• 573+00	-873+00	• 573+00
8	-0.134	-0.325	-0.325	-0.325	• 782	-606+00	-411+00	-411+00	• 782	-606+00	-411+00	• 606+01	• 606+01	• 596+00	-732+00	• 596+00
1.0	-0.218	-0.386	-0.386	-0.386	• 898	-499+00	-353+00	-353+00	• 898	-499+00	-560+01	• 790+01	• 790+01	• 616+00	-611+00	• 616+00
1.2	-0.302	-0.452	-0.452	-0.452	1.012	-409+00	-301+00	-301+00	1.012	-409+00	-756+01	• 103+02	• 103+02	• 634+00	-509+00	• 634+00
1.4	-0.398	-0.522	-0.522	-0.522	1.448	-177+00	-152+00	-152+00	1.448	-177+00	-240+02	• 281+02	• 281+02	-420+00	-420+00	-652+00
1.6	-0.476	-0.594	-0.594	-0.594	1.006	-1.124	-334+00	-255+00	1.006	-1.124	-101+02	• 133+02	• 133+02	-420+00	-420+00	-652+00
1.8	-0.566	-0.668	-0.668	-0.668	1.234	-272+00	-215+00	-215+00	1.234	-272+00	-107+00	• 136+02	• 136+02	-347+00	-347+00	-669+00
2.0	-0.657	-0.743	-0.743	-0.743	1.343	-220+00	-181+00	-181+00	1.343	-220+00	-181+02	• 220+02	• 220+02	-285+00	-285+00	-687+00
2.2	-0.752	-0.819	-0.819	-0.819	1.448	-177+00	-152+00	-152+00	1.448	-177+00	-107+00	• 133+02	• 133+02	-708+00	-708+00	-733+00
2.4	-0.850	-0.896	-0.896	-0.896	1.550	-141+00	-127+00	-127+00	1.550	-141+00	-141+00	• 319+02	• 319+02	-190+00	-190+00	-733+00
2.6	-0.954	-0.971	-0.971	-0.971	1.646	-111+00	-107+00	-107+00	1.646	-111+00	-107+00	• 425+02	• 425+02	-154+00	-154+00	-765+00
2.8	-1.056	-1.046	-1.046	-1.046	1.734	-860-01	-899-01	-899-01	1.734	-860-01	-899-01	• 567+02	• 567+02	-124+00	-124+00	-808+00
3.0	-1.192	-1.120	-1.120	-1.120	1.880	-643-01	-758+02	-758+02	1.880	-643-01	-758+02	• 643+02	• 643+02	-994-01	-994-01	-867+00
3.4	-1.535	-1.288	-1.288	-1.288	1.865	-291-01	-516-01	-516-01	1.865	-291-01	-516-01	• 130+03	• 130+03	-592-01	-592-01	-106+00
3.6	-1.954	-1.629	-1.629	-1.629	1.705	-804-02	-283-01	-283-01	1.705	-804-02	-283-01	• 178+03	• 178+03	-507+02	-507+02	-129+00
3.8	-2.095	-1.548	-1.548	-1.548	1.371	-148-02	-124-01	-124-01	1.371	-148-02	-124-01	• 196+03	• 196+03	-235+02	-235+02	-145+00
4.0	-2.829	-1.908	-1.908	-1.908	1.808	-643-01	-758+02	-758+02	1.808	-643-01	-758+02	• 643+02	• 643+02	-961+01	-961+01	-152+00
4.6	-3.617	-2.300	-2.300	-2.300	0.983	-241-03	-501-02	-501-02	0.983	-241-03	-501-02	-199+03	-199+03	-200+02	-200+02	-155+00
5.0	-4.415	-2.699	-2.301	-2.301	0.585	-384-04	-200+03	-200+03	0.585	-384-04	-200+03	-200+03	-200+03	-200+03	-152+00	

EXACT ZIMM EIGENVALUES
 L_1 LN $1/(LN)$ SUM L1/LP RECIP SUM ((1/LP)2 /LP)2 PHI
 $.941-03$ $.297+01$ $.336+00$ $.225+04$ 2.115 $.473$ $.129+07$ 1.1435 $.256$ 2.308

REDUCED LOG		DYNAMIC LOG		VISCOSITY LOG		MODULUS LOG		MON ETA2/1		H=200 H=15 ARCTAN	
OWTI	ETAIR	ETA2R	G1R	G2R	ETAIR	ETA2R	G1R	G2R	ETAIR	ETA2/1	
-2.8	-325	-2.742	-5.542	-2.475	-212+01	-181-02	-287-05	-335-07	-212+01	-857-03	
-2.0	-325	-1.942	-3.942	-1.675	-212+01	-114-01	-114-03	-212-01	-212+01	-541-02	
-1.8	-325	-1.742	-3.542	-1.475	-211+01	-181-01	-287-03	-335-01	-212+01	-857-02	
-1.4	-325	-1.342	-2.742	-1.075	-211+01	-455-01	-181-02	-841-01	-211+01	-215-01	
-1.0	-323	-0.946	-1.946	-0.677	-210+01	-113+00	-113-01	-210+00	-211+01	-538-01	
-0.8	-320	-0.751	-1.551	-0.480	-209+01	-177+00	-281-01	-331+00	-210+01	-646-01	
-0.6	-313	-0.565	-1.165	-0.287	-205+01	-272+00	-684-01	-516+00	-207+01	-132+00	
-0.4	-295	-0.398	-0.798	-0.105	-197+01	-400+00	-159+00	-785+00	-201+01	-200+00	
-0.2	-259	-0.268	-0.468	-0.059	-182+01	-539+00	-340+00	-115+01	-190+01	-289+00	
0.0	-199	-0.198	-0.198	-0.199	-158+01	-635+00	-635+00	-158+01	-171+01	-381+00	
0.2	-123	-0.189	-0.011	-0.323	-133+01	-647+00	-103+01	-210+01	-148+01	-454+00	
0.4	-043	-0.219	-0.181	-0.443	-111+01	-604+00	-152+01	-278+01	-126+01	-500+00	
0.6	-036	-0.264	-0.336	-0.564	-921+00	-545+00	-217+01	-367+01	-107+01	-534+00	
0.8	-016	-0.317	-0.483	-0.684	-766+00	-482+00	-304+01	-483+01	-905+00	-561+00	
1.0	-197	-0.377	-0.623	-0.803	-635+00	-420+00	-420+01	-635+01	-762+00	-534+00	
1.2	-280	-0.441	-0.759	-0.920	-525+00	-362+00	-574+01	-832+01	-638+00	-604+00	
1.4	-364	-0.508	-0.892	-1.036	-432+00	-310+00	-779+01	-109+02	-532+00	-622+00	
1.6	-450	-0.578	-1.022	-1.150	-355+00	-254+00	-105+02	-141+02	-442+00	-640+00	
1.8	-538	-0.650	-1.150	-1.262	-290+00	-224+00	-141+02	-183+02	-366+00	-658+00	
2.0	-629	-0.723	-1.277	-1.371	-235+00	-189+00	-199+02	-235+02	-302+00	-678+00	
2.2	-722	-0.796	-1.404	-1.478	-190+00	-160+00	-253+02	-300+02	-248+00	-701+00	
2.4	-820	-0.870	-1.530	-1.580	-151+00	-135+00	-339+02	-380+02	-203+00	-729+00	
2.6	-924	-0.942	-1.658	-1.676	-119+00	-114+00	-455+02	-474+02	-165+00	-765+00	
2.8	-1.039	-1.014	-1.786	-1.761	-914-01	-969-01	-611+02	-577+02	-133+00	-814+00	
3.0	-1.171	-1.086	-1.914	-1.829	-675-01	-820+02	-675+02	-106+00	-882+00		
3.4	-1.541	-1.259	-2.141	-1.859	-298-01	-551-01	-138+03	-723+02	-622+01	-109+01	
3.8	-2.137	-1.538	-2.262	-1.663	-730-02	-290-01	-183+01	-461+02	-299-01	-132+01	
4.2	-2.886	-1.906	-2.294	-1.314	-130-02	-124-01	-197+03	-206+02	-125+01	-147+01	
4.6	-3.677	-2.300	-2.300	-0.923	-211-03	-501-02	-199+01	-838+01	-502-02	-153+01	
5.0	-4.475	-2.699	-2.301	-0.525	-335-04	-200-02	-200+03	-335+01	-200-02	-155+01	

EXACT ZINK-EIGENVALUES IN $N=1$

EXACT ZIMM EIGENVALUES		$N=200$		$N=20$	
L1	LN	SUM	RECIP	SUM	PHI
1.17-0.2	2.53+01	3.80+00	1.89+04	2.208	-23
1/(LN)	1/(LPI)	L1/LP	ROCAL	(1/LP)2	2.584
• 1.17-0.2	• 2.53+01	• 3.80+00	• 1.89+04	• 841+06	• 236

REDUCED DYNAMIC VISCOSITY AND MODULUS

EXACT ZIMM EIGENVALUES

EXACT ZIMM EIGENVALUES
 L_1 L_N $1/(LN)$
 L_1/L_P L_N/L_P $1/(LN)$
 SUM RECIP RECIP
 N=200 H*=25
 0.640-0.2*229+0.1*437+0.03
 0.436 2.294
 0.591+0.06 1.1564
 11/1P12 11/1P12
 SUM11 JER PHI
 -23

REDUCED DYNAMIC VISCOSITY AND MODULUS

#1250

-79-

EXACT ZIMM ERGENWALDES
L1 LN EIGENWALDES
145-02 221-01 • 453+00

	SUM	RECIP	SUM	SUM(L1)	JFR	H* = 262
/ (LP)	1 / LP	ROCAL	(1 / LP) 2	LP12	-23	
159 + n4	2. 314	* 432	* 549 + 06	1. 1578	.216	2.855

מונרכיה פוליטית וריבונות אנטומולוגית

LOG	MOD	G1R	G2R	ETAR	ETA2/1	ARCTAN
G2R	ETA18	ETA2R	G1R	G2R	ETAR	MOD
22.436	• 231♦11	• 183-02	• 291-05	• 367-02	• 231♦01	• 793-03
21.636	• 231♦11	• 116-01	• 116-03	• 231-01	• 321♦01	• 500-02
21.475	• 231-01	• 183-01	• 291-03	• 367-01	• 231-01	• 793-02
21.036	• 231-01	• 183-02	• 183-02	• 921-01	• 231-01	• 199-01
-638	• 230+01	• 115+00	• 115+01	• 230+00	• 231+01	• 1698-01
-440	• 229+01	• 180+00	• 285-01	• 363+00	• 230+01	• 783-01
-247	• 225+01	• 276+00	• 693-01	• 566+00	• 227+01	• 122+00
-063	• 217+01	• 406+00	• 162+00	• 864+00	• 221+01	• 185+00
104	• 201+01	• 508+00	• 346+00	• 127+01	• 209+01	• 266+00
250	• 178+01	• 648+00	• 648+00	• 178+01	• 186+01	• 349+00
382	• 152+01	• 666+00	• 105+01	• 241+01	• 156+01	• 413+03
511	• 129+01	• 629+00	• 158+01	• 324+01	• 144+01	• 453+00
898	• 1025	• 658+00	• 403+00	• 638+01	• 106+02	• 78+00
1150	• 563+01	• 353+00	• 229+01	• 437+01	• 124+01	• 482+00
640	• 110+01	• 574+00	• 887+01	• 141+02	• 664+00	• 560+00
770	• 932+00	• 515+00	• 325+01	• 588+01	• 107+01	• 505+00
1.274	• 472+00	• 309+00	• 123+02	• 188+02	• 564+00	• 579+00
1.394	• 393+00	• 270+00	• 457+01	• 790+01	• 913+00	• 630+00
1.811	• 192+00	• 324+00	• 237+00	• 324+02	• 401+00	• 630+00
1.423	• 416-02	• 658+00	• 403+00	• 638+01	• 106+02	• 78+00
1.423	• 118+00	• 142+00	• 865+02	• 745+02	• 184+00	• 877+00
1.750	• 622	• 264+00	• 208+00	• 330+02	• 419+02	• 667+00
1.724	• 211+00	• 183+00	• 461+02	• 526+02	• 279+00	• 716+00
1.811	• 192+00	• 162+00	• 645+02	• 646+02	• 226+00	• 784+00
1.423	• 416-02	• 658+00	• 403+00	• 638+01	• 106+02	• 542+00
1.036	• 118+00	• 142+00	• 865+02	• 745+02	• 184+00	• 877+00
638	• 109-03	• 502-02	• 200+03	• 563+02	• 731-01	• 126+01
238	• 173-04	• 200-02	• 200+03	• 563+02	• 312-01	• 152+01
1.036	• 685-03	• 126-01	• 199+03	• 563+02	• 731-01	• 155+01
638	• 109-03	• 502-02	• 200+03	• 435+01	• 173+01	• 200-02
238	• 173-04	• 200-02	• 200+03	• 173+01	• 200-02	• 156+01

EXACT ZIMM EIGENVALUES
L1 LIN L2 LN I / (LN)
1.163-02 • 1.95+01 • 514+00

EXACT ZIMM EIGENVALUES		N=200		N=30	
L1	LN	1/(LN)	SUM	RECIP	SUM
1.163-02	1.195+01	1.514+00	1.146+04	2.377	4.21
				(1/LP)2	(1/LP)2
				SUM(L1)	JER
					PHI
					-23
					3.002

EXACT ZIMM EIGENVALUES
L1 1/LN

EXACT ZIMM EIGENVALUES		N=300		H*= .05	
L1	LN	SUM	SUM	SUM(L1)	JFR PHI
1/(LP)	1/(LP)	1.838	1.838	(1/LP)2	-23
.240-.03	.366+.01	.273+.00	.786+.04	(1/LP)2	-23
				.194+.08	1.1178
					.314 1.465

REDUCED CYANAMIC VISCOSITY AND MONURUS

ARCTAN									
LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	MON
0WTI	FTAIR	ETA2R	G1R	G2R	ETA1R	ETA2R	G1R	G2R	ETAR
-2.0	-2.8	-2.776	-2.752	-5.552	-2.524	-1.89+01	-1.77-02	-2.99+02	-938+03
-2.0	-2.0	-2.776	-1.952	-3.952	-1.724	-1.95+01	-1.12-01	-1.12-03	-592+02
-1.8	-2.0	-2.776	-1.752	-3.552	-1.524	-1.69+01	-1.77-01	-2.81+03	-938+02
-1.4	-1.4	-2.776	-1.352	-2.752	-1.124	-1.69+01	-4.44+01	-1.77-07	-751+01
-1.0	-1.0	-2.74	-0.956	-1.956	-0.726	-1.68+01	-1.11+00	-1.11-01	-1.98+00
-0.8	-0.8	-2.70	-0.761	-1.561	-0.530	-1.86+01	-0.173+00	-2.75-01	-927+01
-0.6	-0.6	-2.62	-0.576	-1.176	-0.338	-1.83+01	-0.266+00	-6.68-01	-4.59+00
-0.4	-0.4	-2.42	-0.409	-0.809	-0.158	-1.75+01	-0.390+00	-0.155+00	-220+03
-0.2	-0.2	-2.02	-0.281	-0.451	-0.002	-1.59+01	-0.524+00	-0.331+00	-0.101+01
0	0	-1.34	-0.214	-0.214	-0.134	-1.35+01	-0.611+00	-0.136+01	-14.9+01
2	2	-0.047	-0.212	-0.012	-0.247	-1.11+01	-0.614+00	-0.973+00	-1.77+01
4	4	-0.043	-0.250	-0.150	-0.357	-0.975+00	-0.562+00	-1.41+01	-2.27+01
6	6	-0.132	-0.304	-0.296	-0.668	-0.737+00	-0.496+00	-0.197+01	-2.93+01
8	8	-0.222	-0.367	-0.433	-0.573	-0.599+00	-0.429+00	-0.271+01	-3.78+01
0	0	-0.313	-0.437	-0.553	-0.687	-0.495+00	-0.366+00	-0.366+01	-4.86+01
2	2	-0.405	-0.511	-0.689	-0.795	-0.393+00	-0.308+00	-0.489+01	-6.24+01
4	4	-0.493	-0.589	-0.811	-0.902	-0.318+00	-0.248+00	-0.647+01	-7.99+01
6	6	-0.592	-0.670	-0.930	-1.008	-0.256+00	-0.214+00	-0.850+01	-10.2+02
8	8	-0.686	-0.754	1.046	1.114	-0.206+00	-0.176+00	-0.111+02	-1.30+02
0	0	-0.782	-0.840	1.150	1.218	-0.165+00	-0.145+00	-0.145+02	-0.165+02
2	2	-0.878	-0.927	1.273	1.322	-0.132+00	-0.118+00	-0.168+02	-0.210+02
4	4	-0.976	-1.015	1.325	1.424	-0.104+00	-0.095+00	-0.243+02	-0.314+02
6	6	-1.074	-1.103	1.497	1.526	-0.084+00	-0.082+00	-0.957+01	-1.789+01
8	8	-1.276	-1.280	1.720	1.721	-0.052+00	-0.052+00	-0.296+02	-0.421+02
0	0	-1.501	-1.511	1.949	1.988	-0.031+00	-0.031+00	-0.315+01	-0.454+01
2	2	-1.755	-1.792	1.608	1.625	-0.016+00	-0.016+00	-0.525+01	-0.525+02
4	4	-1.074	-1.015	1.608	1.625	-0.058+00	-0.058+00	-0.443+01	-0.443+02
6	6	-1.260	-1.280	1.720	1.721	-0.052+00	-0.052+00	-0.525+01	-0.525+02
8	8	-1.502	-1.511	1.949	1.988	-0.031+00	-0.031+00	-0.791+02	-0.844+02
0	0	-1.619	-1.619	2.181	2.020	-0.166+00	-0.166+00	-0.152+03	-0.105+03
2	2	-1.829	-2.371	1.925	1.925	-0.148+02	-0.148+02	-0.235+03	-0.967+02
4	4	-2.215	-2.371	1.729	1.729	-0.134+02	-0.134+02	-0.285+03	-0.535+02
6	6	-2.871	-2.455	1.350	1.350	-0.126+02	-0.126+02	-0.229+03	-0.297+02
8	8	-2.527	-2.473	1.350	1.350	-0.126+02	-0.126+02	-0.229+03	-0.297+02
0	0	-2.527	-2.473	1.350	1.350	-0.126+02	-0.126+02	-0.229+03	-0.297+02
2	2	-2.527	-2.473	1.350	1.350	-0.126+02	-0.126+02	-0.229+03	-0.297+02
4	4	-2.871	-2.455	1.350	1.350	-0.126+02	-0.126+02	-0.229+03	-0.297+02
6	6	-2.871	-2.455	1.350	1.350	-0.126+02	-0.126+02	-0.229+03	-0.297+02
8	8	-2.527	-2.473	1.350	1.350	-0.126+02	-0.126+02	-0.229+03	-0.297+02
0	0	-2.527	-2.473	1.350	1.350	-0.126+02	-0.126+02	-0.229+03	-0.297+02

EXACT ZIMM EIGENVALUES

LL	LN	1/(LN)	SUM	RECIP	SUM	N=300	H=0.075	PHI
1.349+01	2.87+00	6.644+04	1.967	508	• 1.21+08	1.1273	• 291	1.798

REDUCED DYNAMIC VISCOSITY AND MODULUS

LOG OMT1	LOG ETA2R	G1R	LOG G2R	ETA1R	FTA2R	G1R	62R	ETA2/1	MON	ARCTAN
-2.8	-2.94	-2.748	-5.548	-2.506	• 197+01	283+05	312+02	197+01	• 908-33	
-2.0	-2.94	-1.948	-3.948	-1.706	• 197+01	113+03	197+01	197+01	• 573-02	
-1.8	-2.94	-1.748	-3.548	-1.506	• 197+01	179+01	283+03	179+01	• 908-02	
-1.4	-2.93	-1.349	-2.749	-1.107	• 197+01	448+01	178+07	178+01	• 228-01	
-1.0	-2.92	-0.952	-1.952	-0.708	• 196+01	112+00	112+01	196+00	• 570-01	
-0.8	-2.88	-0.758	-1.558	-0.512	• 194+01	175+00	277+01	308+00	• 898-01	
-0.6	-2.80	-0.572	-1.172	-0.320	• 191+01	268+00	674+01	479+00	• 140+05	
-0.4	-2.61	-0.405	-0.805	-0.139	• 183+01	394+00	157+07	727+00	• 213+00	
-0.2	-2.23	-0.276	-0.476	-0.023	• 167+01	510+00	334+00	105+01	• 307+00	
0.0	-1.58	-0.208	-0.208	-0.158	• 144+01	620+00	620+00	144+01	• 407+00	
0.2	-0.75	-0.203	-0.003	• 275	• 119+01	626+00	992+00	138+01	• 485+00	
0.4	-0.12	-0.238	-0.162	• 388	• 974+00	578+00	145+01	245+01	• 535+00	
0.6	-0.97	-0.289	-0.311	• 503	• 800+00	514+00	205+01	318+01	• 951+00	• 571+00
1.4	-4.50	-0.560	-0.840	• 950	• 355+00	276+00	692+01	892+01	• 794+00	• 660+00
1.6	-5.41	-0.637	-0.953	• 617	• 655+01	448+00	283+01	414+01	• 407+00	• 407+00
1.8	-6.33	-0.717	-1.083	• 586	• 729	• 36+00	385+00	536+01	• 623+00	• 623+00
2.0	-7.26	-0.845	-1.201	• 847	• 847	• 37+00	327+00	519+01	• 694+00	• 694+00
2.2	-8.21	-0.883	-1.317	• 589	• 452	• 38+00	293+01	414+01	• 675+00	• 675+00
2.4	-9.17	-0.967	• 433	• 617	• 617	• 39+00	298+00	918+01	115+02	• 369+00
2.6	-1.015	-1.052	• 548	• 585	• 585	• 40+00	385+00	159+02	147+02	• 302+00
2.8	-1.116	-1.137	• 653	• 684	• 684	• 41+00	460+02	172+01	280+01	• 177+03
3.0	-1.220	-1.221	• 779	• 780	• 780	• 42+00	460+02	162+01	256+03	• 851+01
3.2	-2.21	-0.821	-0.883	• 317	• 379	• 43+00	208+02	240+02	20+00	• 743+00
3.4	-1.452	-1.384	• 016	• 167	• 167	• 44+00	231+00	601+01	601+02	• 851+01
3.6	-1.015	-1.053	• 247	• 2035	• 2035	• 45+00	121+02	413+01	104+03	• 883+00
3.8	-1.765	-1.553	• 408	• 1.930	• 1.930	• 46+00	192+00	353+02	328+01	• 102+01
4.0	-2.270	-1.792	• 408	• 1.623	• 1.623	• 47+00	108+00	271+02	304+02	• 162+00
4.2	-2.977	-2.136	• 464	• 1.623	• 1.623	• 48+00	106+00	188+02	131+00	• 761+00
5.0	-3.759	-2.525	• 475	• 1.241	• 1.241	• 49+00	105+02	731+02	291+03	• 420+02
				• 174+03	• 299+02	• 299+03	174+02	299+02	174+02	• 143+01

EXACT ZIMM EIGENVALUES
 L_1 $\ln 1/(L_1)$ $\sum 1/(L_1)$
 $\cdot 372-33 \cdot 332+01 \cdot 302+00 \cdot 547+04$

$N=300$ $H=10$
 $\sum L_1/LP_1$ L_1/LP $RECIP$
 $(1/LP)_1^2$ $(LP)_2$ JER
 $\cdot 821+07 \cdot 1.1349 \cdot 274$ 2.038 -23

REDUCED DYNAMIC VISCOSITY AND MODULUS

LOG	LOG	LOG	LOG	LOG	LOG	OMT	ETAIR	ETABR	G1A	G2R	ETAIR	ETABR	G1R	G2R	ETAIR	ETAR	M00	ARCTAN	ETA2/1
-2.8	-0.308	-2.745	-5.545	-2.492	-0.203+01	-180-02	-285-05	-322-02	-0.203+01	-203+01	-884-03	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01
-2.0	-0.308	-1.945	-3.945	-1.692	-0.203+01	-113-01	-113-01	-113-01	-0.203+01	-203+01	-55-02	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01
-1.8	-0.308	-1.745	-3.545	-1.492	-0.203+01	-180-01	-285-03	-322-01	-0.203+01	-203+01	-884-02	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01
-1.4	-0.308	-1.346	-2.746	-1.092	-0.203+01	-451-01	-180-02	-809-01	-0.203+01	-203+01	-222-01	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01	-203+01
-1.0	-0.306	-0.943	-1.949	-0.694	-0.202+01	-112-01	-112-01	-202+00	-0.202+00	-202+00	-555-01	-202+00	-202+00	-202+00	-202+00	-202+00	-202+00	-202+00	-202+00
-0.8	-0.303	-0.755	-1.555	-0.497	-0.201+01	-176+00	-279-01	-318+00	-0.202+01	-202+01	-874-01	-202+01	-202+01	-202+01	-202+01	-202+01	-202+01	-202+01	-202+01
-0.6	-0.295	-0.569	-1.169	-0.305	-0.197+01	-270+00	-678-01	-495+00	-0.199+01	-199+01	-136+00	-199+01	-199+01	-199+01	-199+01	-199+01	-199+01	-199+01	-199+01
-0.4	-0.277	-0.401	-0.801	-0.123	-0.189+01	-397+00	-158+01	-753+00	-0.193+01	-193+01	-207+00	-193+01	-193+01	-193+01	-193+01	-193+01	-193+01	-193+01	-193+01
-0.2	-0.240	-0.272	-0.472	-0.040	-0.174+01	-534+00	-337+00	-110+01	-0.162+01	-162+01	-298+00	-110+01	-110+01	-110+01	-110+01	-110+01	-110+01	-110+01	-110+01
0	-0.177	-0.203	-0.203	-0.177	-0.150+01	-627+00	-627+00	-150+01	-0.163+01	-163+01	-395+00	-150+01	-150+01	-150+01	-150+01	-150+01	-150+01	-150+01	-150+01
2	-0.097	-0.197	-0.003	-0.297	-0.125+01	-636+00	-101+01	-198+01	-0.140+01	-140+01	-470+00	-101+01	-101+01	-101+01	-101+01	-101+01	-101+01	-101+01	-101+01
4	-0.014	-0.229	-0.171	-0.414	-0.103+01	-590+00	-590+00	-148+01	-0.119+01	-119+01	-519+00	-590+00	-590+00	-590+00	-590+00	-590+00	-590+00	-590+00	-590+00
6	-0.069	-0.277	-0.323	-0.531	-0.0854+00	-528+00	-528+00	-210+01	-0.100+01	-100+01	-554+00	-528+00	-528+00	-528+00	-528+00	-528+00	-528+00	-528+00	-528+00
8	-0.152	-0.534	-0.456	-0.648	-0.0705+00	-464+00	-464+00	-464+00	-0.445+01	-445+01	-582+00	-464+00	-464+00	-464+00	-464+00	-464+00	-464+00	-464+00	-464+00
0	-0.237	-0.397	-0.603	-0.763	-0.0580+00	-401+00	-401+00	-401+00	-0.580+01	-580+01	-705+00	-401+00	-401+00	-401+00	-401+00	-401+00	-401+00	-401+00	-401+00
2	-0.322	-0.465	-0.735	-0.878	-0.0476+00	-343+00	-544+01	-754+01	-0.754+01	-754+01	-605+00	-343+00	-544+01	-754+01	-754+01	-754+01	-754+01	-754+01	-754+01
4	-0.410	-0.536	-0.864	-0.990	-0.0389+00	-291+00	-731+01	-978+01	-0.731+01	-978+01	-605+00	-291+00	-731+01	-978+01	-978+01	-978+01	-978+01	-978+01	-978+01
6	-0.498	-0.611	-0.989	-1.102	-0.0318+00	-245+00	-975+01	-126+02	-0.975+01	-126+02	-605+00	-245+00	-975+01	-126+02	-126+02	-126+02	-126+02	-126+02	-126+02
8	-0.588	-0.688	-1.112	-1.212	-0.0258+00	-205+00	-129+02	-163+02	-0.129+02	-163+02	-605+00	-205+00	-129+02	-163+02	-163+02	-163+02	-163+02	-163+02	-163+02
0	-0.679	-0.766	-1.234	-1.321	-0.0209+00	-171+00	-171+02	-209+02	-0.171+02	-209+02	-605+00	-171+00	-171+02	-209+02	-209+02	-209+02	-209+02	-209+02	-209+02
2	-0.772	-0.847	-1.353	-1.428	-0.169+00	-142+00	-226+02	-268+02	-0.226+02	-226+02	-605+00	-169+00	-142+00	-226+02	-226+02	-226+02	-226+02	-226+02	-226+02
4	-0.857	-0.928	-1.472	-1.533	-0.136+00	-118+00	-297+02	-341+02	-0.297+02	-341+02	-605+00	-136+00	-118+00	-297+02	-297+02	-297+02	-297+02	-297+02	-297+02
6	-0.964	-1.209	-1.591	-1.636	-0.109+00	-97-01	-390+02	-432+02	-0.390+02	-432+02	-605+00	-97-01	-118+03	-432+02	-432+02	-432+02	-432+02	-432+02	-432+02
8	-1.065	-1.090	-1.710	-1.775	-0.0861+01	-81-01	-513+02	-543+02	-0.513+02	-543+02	-605+00	-81-01	-81-01	-513+02	-513+02	-513+02	-513+02	-513+02	-513+02
0	-1.171	-1.170	-1.870	-1.929	-0.0674+01	-67-01	-676+02	-674+02	-0.676+02	-674+02	-605+00	-118+03	-118+03	-676+02	-676+02	-676+02	-676+02	-676+02	-676+02
2	-1.415	-1.327	-2.073	-1.985	-0.385-01	-47-01	-471-01	-967+02	-0.471-01	-967+02	-608+00	-118+03	-118+03	-471-01	-471-01	-471-01	-471-01	-471-01	-471-01
4	-1.766	-1.502	-2.298	-2.034	-0.172-01	-31-01	-315-01	-108+03	-0.172-01	-108+03	-734+00	-199+03	-199+03	-315-01	-315-01	-315-01	-315-01	-315-01	-315-01
6	-2.334	-1.763	-2.431	-1.866	-0.464-02	-17-01	-270+03	-735+02	-0.270+03	-735+02	-734+00	-176-01	-176-01	-270+03	-270+03	-270+03	-270+03	-270+03	-270+03
8	-3.072	-2.131	-2.469	-1.528	-0.848-03	-73-02	-294+03	-338+02	-0.294+03	-338+02	-734+00	-744-02	-744-02	-294+03	-294+03	-294+03	-294+03	-294+03	-294+03
0	-3.861	-2.524	-2.476	-1.139	-0.138-03	-299-02	-299+03	-138+02	-0.299+03	-138+02	-299+02	-138+02	-299+03	-138+02	-138+02	-138+02	-138+02	-138+02	-138+02

EXACT ZIMM EIGENVALUES

L1	LN	1/(LN)	SUM	RECIP	SUM	SUM(L1)	JER	PHI
		1/(LP1)	L1/LP	ROCAL	(1/LP) ²	/LP1 ²	-23	
•451-03	•311+01	•322+00	.466+04	2.102	.476	.561+07	1.1417	•258 2.258

REDUCED DYNAMIC VISCOSITY AND MODULUS

LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG
OMT1	FTAIR	ETA2R	G1R	G2R	ETA2R	G1R	G2R	ARCTAN
-2.8	-323	-2.742	-5.542	-2.477	-210+01	-181-02	-287-05	•333-02
-2.0	-323	-1.942	-3.942	-1.677	-210+01	-114-01	-210-01	•210+01
-1.8	-323	-1.743	-3.543	-1.477	-210+01	-161-01	-287-03	•333-01
-1.4	-322	-1.343	-2.743	-1.078	-210+01	-454-01	-181-02	•861-02
-1.0	-321	-0.946	-1.946	-0.679	-209+01	-113+00	-113-01	•216-01
-0.8	-317	-0.752	-1.552	-0.483	-208+01	-177+00	-281-01	•209+01
-0.6	-310	-0.566	-1.166	-0.290	-204+01	-272+00	-683-01	•513+00
-0.4	-292	-0.399	-0.799	-0.108	-196+01	-399+00	-159+00	•780+00
-0.2	-256	-0.269	-0.469	0.055	-180+01	-548+00	-340+00	•114+01
0.0	-196	-0.199	-0.199	-0.196	-157+01	-633+00	-633+00	•157+01
0.2	-119	-0.191	0.019	0.319	-131+01	-645+00	-102+01	•208+01
0.4	-039	-0.221	0.179	0.479	-109+01	-601+00	-151+01	•275+01
0.6	-041	-0.267	0.233	0.559	-911+00	-541+00	-215+01	•352+01
0.8	-121	-0.321	0.479	0.679	-757+00	-478+00	-301+01	•479+01
1.0	-202	-0.381	0.619	0.798	-627+00	-416+00	-116+01	•627+01
1.2	-285	-0.446	0.754	0.915	-518+01	-358+00	-568+01	•822+01
1.4	-369	-0.514	0.886	1.031	-427+00	-306+00	-768+01	•107+02
1.6	-455	-0.586	1.014	1.145	-351+00	-260+00	-103+02	•140+02
1.8	-542	-0.659	1.141	1.258	-287+00	-219+00	-138+02	•181+02
2.0	-631	-0.734	1.266	1.369	-234+00	-184+00	-184+02	•234+02
2.2	-722	-0.810	1.390	1.478	-190+00	-155+00	-574+02	•612+02
2.4	-815	-0.887	1.513	1.586	-153+00	-130+00	-326+02	•384+02
2.6	-912	-0.964	1.636	1.698	-122+00	-109+00	-432+02	•468+02
2.8	-1013	-1.041	1.759	1.787	-970-01	-910-01	-574+02	•612+02
3.0	-1122	-1.116	1.884	1.878	-756-01	-765-01	-765+02	•756+02
3.4	-1382	-1.267	2.133	2.018	-415-01	-541-01	-136+03	•104+03
3.8	-1783	-1.454	2.346	2.017	-165-01	-351-01	-222+03	•104+03
4.2	-2.412	-1.752	2.448	1.788	-387-02	-177-01	-280+03	•614+02
4.6	-3.172	-2.128	2.472	1.428	-673-03	-745-02	-297+03	•268+02
5.0	-3.966	-2.524	2.476	1.034	-108-03	-299-02	-299+01	•108+02

EXACT ZIMM EIGENVALUES
 L_1 $\ln(1/L_1)$ $1/(LN)$ SUM
 $1/(LP)$ L_1/LP $ROCAL$
• 504-03 • 297+01 • 336+00 • 425+04 2.143 -467

N=300 H=± .15
 SUM $SUM(L_1)$ JER PHI
 $(1/LP)_2$ $/LP)_2$ -23
• 451+07 • 1.1454 .249 2.377

REDUCED DYNAMIC VISCOSITY AND MODULUS

LOG	LOG	LOG	LOG	LOG	LOG	OMRI	FTA1R	ETA2R	G1R	ETA1R	ETA2R	G1R	G2R	MOD	ARCTAN	FTA2/1
-2.8	-3.1	-2.741	-5.561	-2.468	-2.14+01	-1.92-02	-2.88-05	-340-02	-214+01	-214-01	-214+01	-214-01	-847-03			
-2.0	-3.1	-1.941	-3.941	-1.656	-2.14+01	-1.15-01	-1.15-03	-214-01	-214+01	-214-01	-214+01	-214-01	-515-02			
-1.8	-3.1	-1.741	-3.541	-1.469	-2.14+01	-1.81-01	-2.88-03	-340-01	-214+01	-214-01	-214+01	-214-01	-847-02			
-1.4	-3.1	-1.342	-2.742	-1.069	-2.14+01	-4.55-01	-1.81-02	-852-01	-214+01	-213-01	-213-01	-213-01	-213-01			
-1.0	-3.0	-1.329	-1.945	-1.945	-6.71	-2.13+01	-1.14+00	-1.14-01	-213+00	-213+00	-213+00	-213+00	-213+00	-213+00		
-0.8	-3.26	-7.51	-1.551	-4.74	-2.12+01	-1.78+00	-2.81-01	-336+00	-212+01	-212+01	-212+01	-212+01	-837-01			
-0.6	-3.18	-5.64	-1.164	-2.82	-2.08+01	-2.73+00	-1.5-01	-523+00	-210+01	-210+01	-210+01	-210+01	-130+00			
-0.4	-3.01	-3.97	-7.97	-0.99	-2.00+01	-4.01+00	-1.60+00	-796+00	-204+01	-198+00	-204+01	-198+00				
-0.2	-2.66	-2.67	-4.67	-0.65	-1.84+01	-5.41+00	-341+00	-116+01	-192+01	-285+00	-285+00	-285+00				
0	-2.07	-1.96	-1.96	-0.207	-1.61+01	-6.16+00	-6.36+00	-161+01	-173+01	-376+00	-376+00	-376+00				
2	-1.31	-1.88	-0.12	-0.2	-1.35+01	-6.49+00	-1.03+01	-215+01	-150+01	-447+00	-447+00	-447+00				
4	-0.53	-2.17	-1.83	-4.53	-1.13+01	-6.07+00	-1.53+01	-284+01	-128+01	-524+00	-524+00	-524+00				
6	-0.24	-2.61	-2.39	-5.76	-0.945+00	-5.48+00	-2.18+01	-376+01	-109+00	-657+00	-657+00	-657+00				
8	-1.03	-3.14	-4.86	-6.97	-7.89+00	-4.96+00	-306+01	-498+01	-927+00	-552+00	-552+00	-552+00				
10	-1.83	-3.72	-6.28	-8.17	-6.57+00	-4.24+00	-107+02	-148+02	-782+00	-573+00	-573+00	-573+00				
12	-2.63	-4.6	-7.54	-9.37	-5.45+00	-3.67+00	-1.818	-1.818	-104+00	-646+02	-524+02	-524+02				
14	-3.46	-5.52	-8.98	-1.054	-4.51+00	-3.15+00	-790+01	-113+02	-550+00	-609+00	-609+00	-609+00				
16	-4.29	-5.71	-1.029	-1.171	-3.72+00	-2.8+00	-1.44+02	-193+02	-381+00	-641+00	-641+00	-641+00				
18	-5.15	-6.43	-1.157	-1.285	-3.09+00	-2.28+00	-1.16+02	-460+02	-524+00	-720+00	-720+00	-720+00				
20	-6.02	-7.15	-1.398	-2.50+00	-1.93+00	-1.93+02	-258+02	-322+02	-322+02	-322+02	-322+02	-322+02				
22	-6.92	-7.89	-1.411	-1.917	-1.008	-809+01	-826+01	-806+02	-116+00	-796+00	-796+00	-796+00				
24	-7.84	-8.63	-1.537	-1.616	-1.64+00	-1.37+00	-1.37+02	-431+01	-589+01	-108+03	-108+03	-108+03				
26	-8.80	-9.37	-1.663	-1.720	-1.72+00	-1.66+00	-1.66+02	-431+01	-589+01	-729+01	-729+01	-729+01				
28	-9.82	-1.011	-1.739	-1.818	-1.818	-1.818	-1.818	-158+01	-372+01	-372+01	-372+01	-372+01				
30	-1.092	-1.092	-1.083	-1.083	-1.083	-1.083	-1.083	-158+01	-372+01	-372+01	-372+01	-372+01				
32	-1.366	-1.230	-2.170	-2.034	-2.034	-2.034	-2.034	-158+01	-372+01	-372+01	-372+01	-372+01				
34	-1.366	-1.230	-2.170	-2.034	-2.034	-2.034	-2.034	-158+01	-372+01	-372+01	-372+01	-372+01				
36	-1.803	-1.430	-2.370	-1.097	-1.097	-1.097	-1.097	-158+01	-372+01	-372+01	-372+01	-372+01				
38	-2.463	-1.745	-2.455	-1.737	-1.737	-1.737	-1.737	-158+01	-372+01	-372+01	-372+01	-372+01				
40	-3.234	-2.127	-2.473	-1.366	-1.366	-1.366	-1.366	-158+01	-372+01	-372+01	-372+01	-372+01				
42	-4.029	-2.523	-2.477	-9.71	-9.71	-9.71	-9.71	-9.71	-300+02	-300+03	-936+01	-936+01	-936+01			

EXACT ZIMM EIGENVALUES
 L_1 $\ln \frac{1}{(L_1)}$

EXACT ZIMM EIGENVALUES		$N=300$		$N=20$	
L_1	\ln	$1/(LN)$	SUM	RECIP	SUM
1/(LP)	1/(LP)	1/(LP)	1/(LP)	ROCAL	SUM(LP)12
0.633-0.3	0.263+0.1	0.380+0.0	0.352+0.4	2.229	0.449
					•287+0.7
					1.1516
					•232
					2.6222
					-2.3
					PHI

REDUCED DYNAMIC VISCOSITY

EXACT ZIMM EIGENVALUES
 $L_1 \ln \frac{1}{(LN)}$
 $-764-0.3 -229+0.1 -637+0.0$

EXACT ZIMM EIGENVALUES					
L_1	$\ln(1/LN)$	SUM	$RECIP$	SUM	$N=300$
1.764-03	• 2229+01	• 437+00	.302+04	22.308	• 433
			1/LP	1/(LP)	1/(LP)
			ROCAL	(1/LP)2	(1/LP)1
				• 198+07	• 1.1564
					• 217
					2.814
					-23
					PHI
					• 25

REDUCED DYNAMIC VISCOSITY AND HIGH-SUS

EXACT ZIMM EIGENVALUES
 L_1 \ln $1/(LN)$
 $1/(LP)$
 $\cdot 795 \cdot 0 \cdot 221 \cdot 0 \cdot 1 \cdot 453 \cdot 0 \cdot 0 \cdot 293 \cdot 0 \cdot 4$

N=300 H=262
 L_1 L_1/LP RECIP SUM(L1) JER PHI
 $2 \cdot 326$ $\cdot 430$ $(1/LP)^2$ $/LP^2$ -23
 $\cdot 183 \cdot 0 \cdot 7$ $1 \cdot 157 \cdot 3$ $\cdot 214$ $2 \cdot 856$

REDUCED DYNAMIC VISCOSITY AND MONULUS									
LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG	LOG
OMT1	ETA1R	ETA2R	G1R	G2R	ETA1R	ETA2R	G1R	G2R	ARCTAN
-2.8	-367	-2.737	-5.537	-2.433	-233+01	-183-02	-291-05	-369-02	M00
-2.0	-367	-1.937	-3.937	-1.633	-233+01	-116-01	-116-03	-233-01	ETA2/1
-1.8	-367	-1.737	-3.537	-1.433	-233+01	-183-01	-291-03	-369-01	789-03
-1.4	-366	-1.337	-2.737	-1.034	-232+01	-450-01	-183-02	-925-01	498-02
-1.0	-365	-0.940	-1.940	-0.635	-232+01	-115+00	-115+01	-232+00	788-02
-0.8	-362	-0.746	-1.546	-0.438	-230+01	-179+00	-284-01	-365+00	-198-01
-0.6	-355	-0.560	-1.160	-0.245	-226+01	-276+00	-692-01	-569+00	-495-01
-0.4	-339	-0.392	-0.792	-0.061	-218+01	-406+00	-161+00	-869+00	-231+01
-0.2	-307	-0.261	-0.461	-0.107	-203+01	-548+00	-346+00	-128+01	-779-01
0	-253	-0.189	-0.189	-0.023	-179+01	-647+00	-647+00	-179+01	-347+00
2	-185	-0.177	-0.177	-0.020	-198	-515	-153+01	-665+00	-105+01
4	-115	-0.202	-0.202	-0.035	-130+01	-628+00	-158+01	-327+01	-167+01
6	-64.5	-0.242	-0.242	-0.058	-111+01	-573+00	-228+01	-442+01	-410+00
8	-0.024	-0.289	-0.289	-0.051	-776	-945+00	-514+00	-324+01	-516+00
0	-0.095	-0.341	-0.341	-0.065	-905	-804+00	-456+00	-456+01	-449+00
2	-0.166	-0.397	-0.397	-0.080	-803	-1.034	-682+00	-401+00	-327+01
4	-0.239	-0.455	-0.455	-0.094	-1.161	-577+00	-351+00	-531+00	-442+01
6	-0.313	-0.514	-0.514	-0.108	-1.287	-487+00	-306+00	-28+01	-531+00
8	-0.389	-0.574	-0.574	-0.122	-1.411	-408+00	-267+00	-168+02	-546+00
0	-0.467	-0.634	-0.634	-0.136	-1.533	-341+00	-232+00	-232+02	-561+00
2	-0.549	-0.693	-0.693	-0.150	-1.651	-282+00	-203+00	-322+02	-578+00
4	-0.636	-0.750	-0.750	-0.165	-1.764	-2.032	-108+00	-122+01	-598+00
6	-0.731	-0.805	-0.805	-0.180	-1.795	-1.869	-1.960	-1.57+00	-623+00
8	-0.839	-0.859	-0.859	-0.194	-1.941	-1.961	-1.95+00	-1.38+00	-656+00
0	-0.968	-0.915	-0.915	-0.209	-2.095	-2.032	-1.08+00	-1.22+01	-696+00
2	-1.035	-1.072	-1.072	-0.233	-2.328	-2.048	-444-01	-847-01	-701+00
4	-1.197	-1.356	-1.356	-0.244	-1.827	-1.06-01	-440-01	-278+03	-109+01
6	-1.272	-1.729	-1.729	-0.247	-1.471	-1.468	-1.85-02	-187-01	-147+01
8	-1.352	-2.124	-2.124	-0.247	-1.075	-2.99-03	-752-02	-299+03	-153+01
0	-1.432	-2.523	-2.523	-0.247	-0.677	-4.75-04	-300-02	-300+03	-155+01

EXACT ZIMM EIGENVALUES

L_1	\ln	$1/(1\ln)$	SUM	SUM	RECIP	SUM	SUM(L_1)	$H=30$	PHI
-892-03	.195+01	.514+30	.267+n4	2.382	.420	.146+07	1.1596	.204	2.983

REDUCED DYNAMIC VISCOSITY AND MODULUS

LOG	LOG	LOG	LOG	G1R	G2R	ETA1R	ETA2R	G1R	G2R	MOD	ARCTAN
-2.8	-377	-2-7.36	-5-5.36	-2-4.23	-2-3.8+01	-184-02	-291-05	-377-02	-238+01	-772-03	
-2.0	-377	-1-9.36	-3-9.36	-1-6.23	-2-3.8+01	-116-01	-116-03	-238-01	-238+01	-487-02	
-1.8	-377	-1-7.36	-3-5.36	-1-4.23	-2-3.8+01	-184-01	-291-03	-377-01	-238+01	-772-02	
-1.4	-377	-1-3.36	-2-7.36	-1-0.23	-2-3.8+01	-461-01	-184-02	-948-01	-238+01	-194-01	
-1.0	-375	-1-9.39	-1-9.39	-6.25	-2-3.7+01	-115+00	-115-01	-237+00	-237+01	-484-01	
-0.8	-372	-1-7.45	-1-5.45	-4.28	-2-3.6+01	-180+00	-285-01	-373+00	-236+01	-762-01	
-0.5	-365	-1-5.39	-1-1.59	-2.35	-2-3.2+01	-276+00	-694-01	-583+00	-234+01	-118+00	
-0.4	-350	-1-3.91	-1-7.91	-0.50	-2-2.4+01	-406+00	-162+00	-891+00	-228+01	-180+00	
-0.2	-318	-1-2.60	-1-4.60	-1.18	-2-0.8+01	-549+00	-347+00	-131+01	-215+01	-258+00	
0.0	-266	-1-1.88	-1-1.88	-2.66	-1-1.85+01	-649+00	-649+00	-185+01	-196+01	-338+00	
0.2	-200	-1-1.75	-1-0.25	-4.00	-1-1.59+01	-668+00	-106+01	-251+01	-172+01	-399+00	
0.4	-132	-1-1.99	-2.01	-5.32	-1-1.16+01	-632+00	-159+01	-341+01	-150+01	-436+00	
0.6	-065	-1-2.38	-3.52	-6.65	-1-1.16+01	-578+00	-230+01	-463+01	-130+01	-462+00	
0.8	-002	-1-2.84	-5.16	-7.98	-1-0.996+00	-520+00	-328+01	-628+01	-112+01	-841+00	
1.0	-069	-1-3.34	-6.66	-9.31	-8.52+00	-463+00	-463+01	-852+01	-970+00	-498+00	
1.2	-138	-1-3.88	-8.12	-1-0.62	-7.28+00	-409+00	-648+01	-115+02	-835+00	-512+00	
1.4	-207	-1-4.44	-9.56	-1-1.93	-6.21+00	-360+00	-904+01	-156+02	-717+00	-526+00	
1.6	-278	-1-5.00	-1-1.00	-1-3.22	-5.27+00	-316+00	-126+02	-210+02	-615+00	-540+00	
1.8	-350	-1-5.56	-1-2.44	-1-4.50	-4.46+00	-278+00	-175+02	-282+02	-526+00	-557+00	
2.0	-426	-1-6.11	-1-3.89	-1-5.74	-3.75+00	-245+00	-245+02	-375+02	-44+00	-579+00	
2.2	-505	-1-6.63	-1-5.37	-1-6.95	-3.13+00	-217+00	-344+02	-495+02	-381+00	-607+00	
2.4	-590	-1-7.14	-1-6.86	-1-8.10	-2.57+00	-193+00	-486+02	-645+02	-322+00	-645+00	
2.6	-685	-1-7.61	-1-8.39	-1-9.15	-2.06+00	-173+00	-690+02	-821+02	-269+00	-699+00	
2.8	-797	-1-8.08	-1-9.92	-2.003	-1-159+00	-156+00	-981+02	-101+03	-223+00	-773+00	
3.0	-938	-1-8.61	-2-1.39	-2-0.62	-1-15+00	-138+00	-138+03	-115+03	-180+00	-874+00	
3.4	-1-376	-1-0.34	2-366	2-0.24	-4.21-01	-925-01	-232+01	-106+03	-102+00	-114+01	
3.6	-2-0.45	-1-3.45	2-455	1-7.55	-902-02	-451-01	-285+03	-569+02	-460-01	-137+01	
4.0	-2-6.18	-1-7.27	2-473	1-3.82	-1-152-02	-188-01	-297+03	-241+02	-188-01	-149+01	
4.6	-3-6.13	-2-1.23	2-477	1-9.87	-2-244-03	-753-02	-300+03	-970+01	-753-02	-154+01	
5.0	-4-4.12	-2-5.23	2-477	1-5.68	-3-387-04	-300-02	-300+03	-387+01	-300-02	-156+01	